# INSTITUTE OF PLASMA PHYSICS OF THE CZECH ACADEMY OF SCIENCES INTRODUCTION TO ENERGY PRINCIPLE, INTERNAL KINK & SAWTOOTH RECONNECTION THEORY AND MODELLING

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## FABIEN JAULMES





## **Overview of this lecture**

- Safety factor profile in tokamaks
- Introduction to the internal kink and the sawtooth crash
- Energy principle and derivation of linear growth rate of internal kink
- Reconnecting magnetic flux based on ideal MHD for poloidal mapping
- Computationally efficient poloidal mapping of the flux and the electric potential

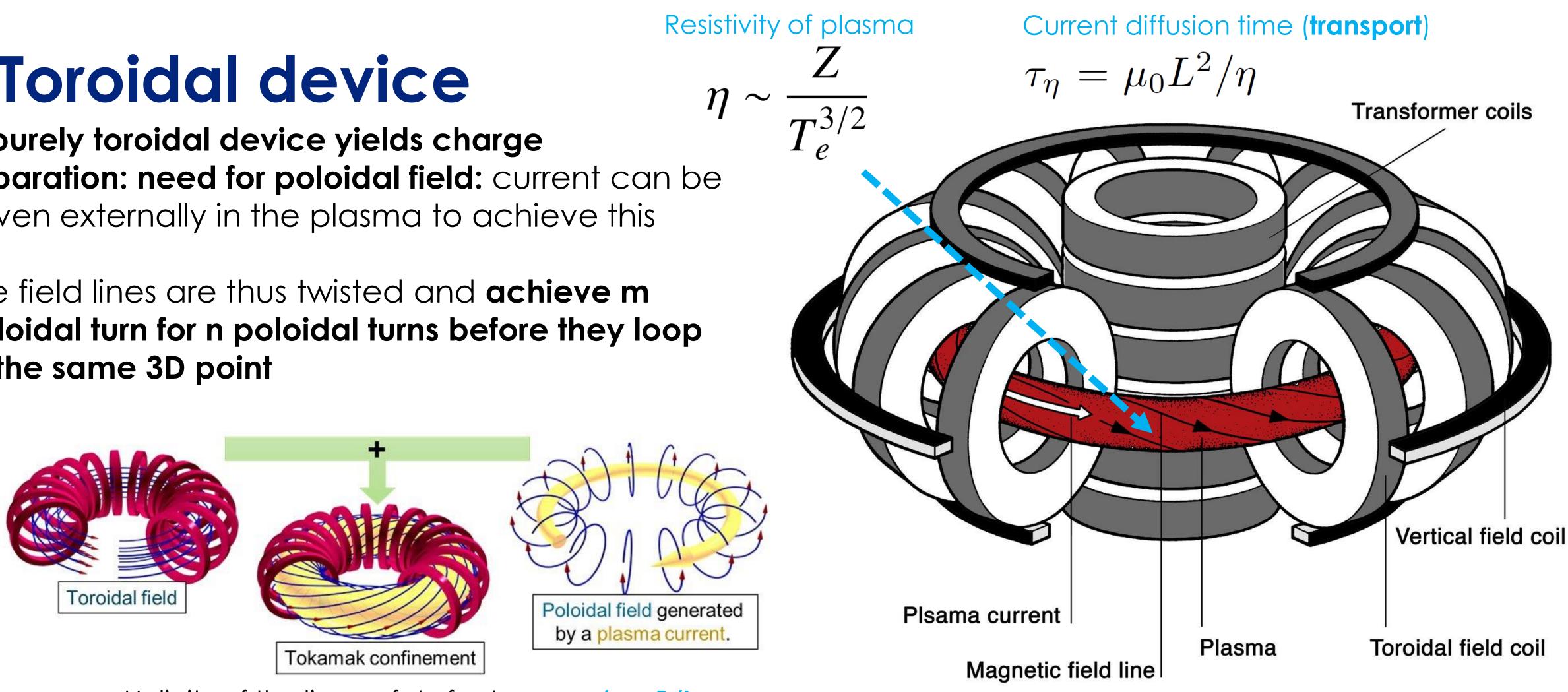






# **Toroidal device**

- A purely toroidal device yields charge separation: need for poloidal field: current can be driven externally in the plasma to achieve this
- The field lines are thus twisted and **achieve m** poloidal turn for n poloidal turns before they loop to the same 3D point



Helicity of the line: safety factor  $q=m/n \sim B/I_p$ 

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## **PRINCIPLES OF TOROIDAL MAGNETIC CONFINEMENT**







# Safety factor profile

• The poloidal field of a toroidally symmetric device can be described by the angular poloidal flux map:

 $\Psi = \Psi(R,Z)$ , so that we express the equilibrium field as:

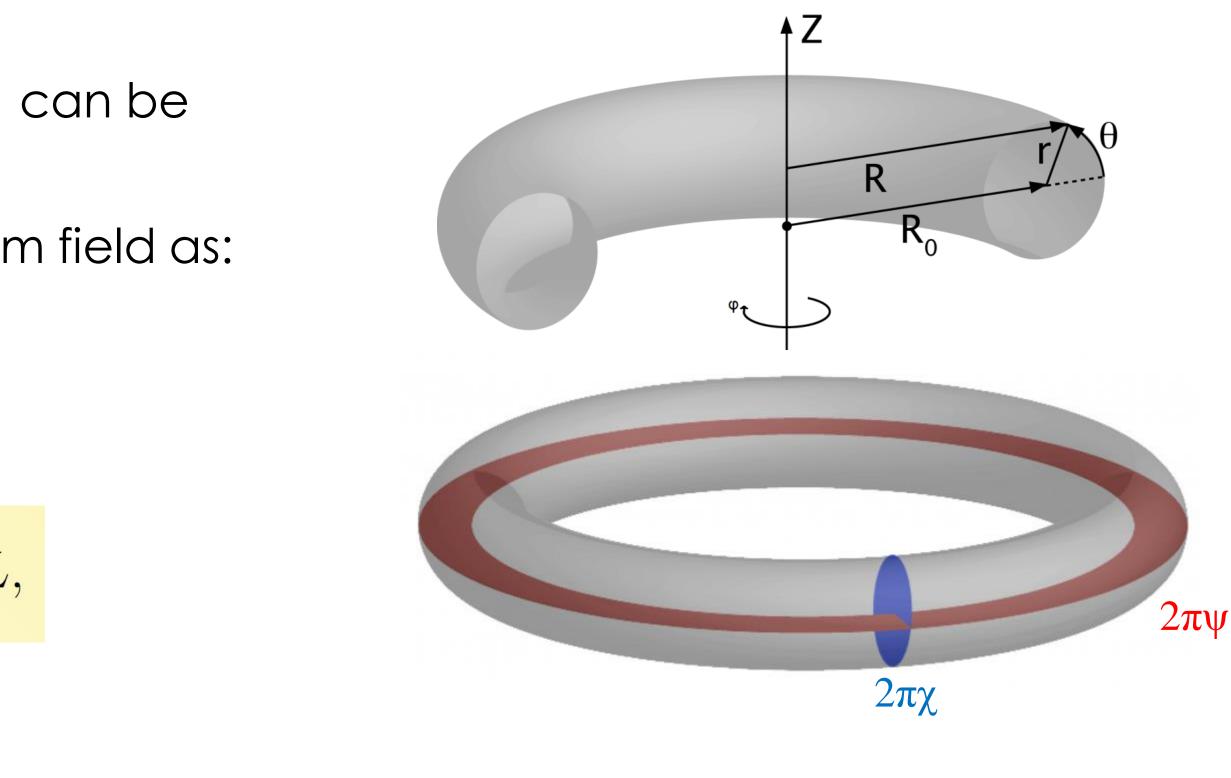
$$\mathbf{B}_{\mathbf{0}} = \nabla \varphi \times \nabla \psi_0 + \frac{1}{R} B_t(R, Z) \nabla \varphi$$

- Angular toroidal flux  $\chi$  can be expressed as:  $2\pi\chi = \iint B_t \, dR \, dZ = \int d\psi_0 \, \oint \, \frac{B_t}{|\nabla\psi_0|} \, dL,$
- We define the local helicity of the field line as: ullet

$$q = \frac{m}{n} = \frac{\mathrm{d}\varphi}{\mathrm{d}\theta} = \frac{\mathrm{d}\chi}{\mathrm{d}\psi}$$

### SAFETY FACTOR PROFILE

Tokamak cylindrical coordinates  $(R,Z,\varphi)$ 



Straight field line angle:

$$\theta = \int \frac{B_t}{|\nabla \chi|} \, dL$$
$$\Phi$$



4/13



# Safety factor profile

There are several basic values which can be measured in the experiment and characterize MHD instability in tokamaks:

- growth rate of the mode  $(\gamma)$ ,
- mode numbers (m, n),
- mode frequency in the laboratory frame  $(\omega)$ ,
- radial structure of the eigenfunction  $(\hat{\xi}_r(\rho))$ , where  $\rho$  is the radial coordinate.

 $\xi(\rho,\theta,\phi,t) = \hat{\xi}_r(\rho) \cdot \cos(m\theta - n\phi + \omega t) \cdot e^{\gamma t}$ 

 $\boldsymbol{\xi} = \boldsymbol{\xi}_0 \exp(i\omega t)$ 

### SAFETY FACTOR PROFILE







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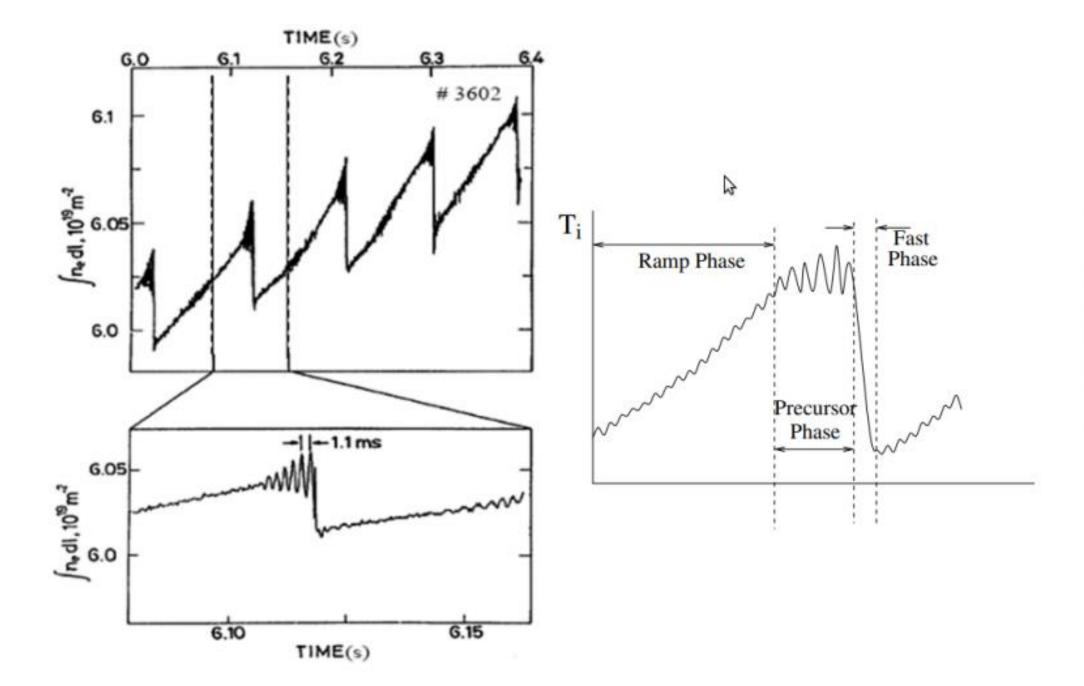
### **INTRODUCTION TO INTERNAL KINK AND SAWTOOTH**







## **Experimental patterns of kink and sawtooth**



[1] I T Chapman 2011 Plasma Phys. Control. Fusion 53 013001

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### **INTRODUCTION TO THE INTERNAL KINK AND THE SAWTOOTH** CRASH

The line-integrated electron density of an early JET sawtoothing plasma. The sawtooth oscillation typically consists of a ramp phase, then a precursor oscillation followed by the fast collapse phase.





## **Experimental patterns of kink and sawtooth**

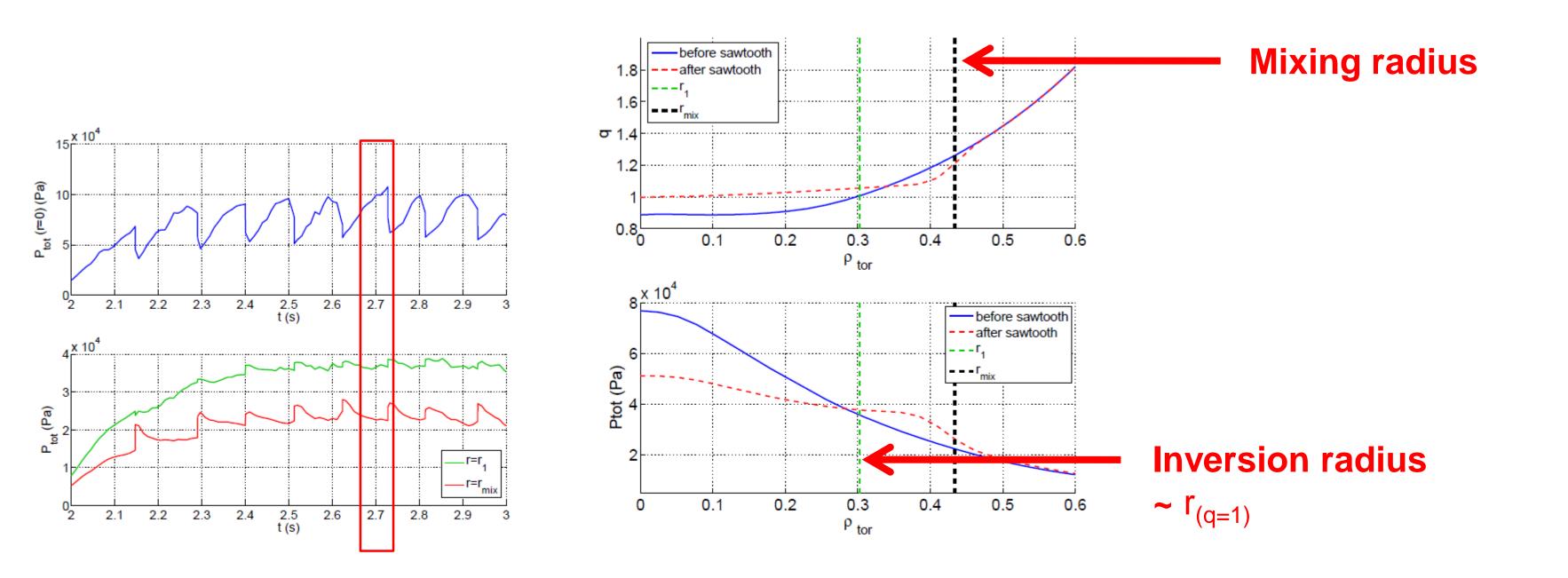


FIGURE 1.4: Left figure: Time evolution of the reconstructed total pressure in an ASDEX Upgrade experiment (discharge #30382). The evolution of the pressure is given at different radial position, displayed in the right figure. The characteristic shape of the evolution of the pressure in the core gave its name to the phenomenon. The radial position where the pressure is not modified by the crash (close to q = 1) is often called the 'inversion radius'. Right figure: evolution of the radial profiles of the safety factor corresponding to the sawtooth crash happening at 2.51s.

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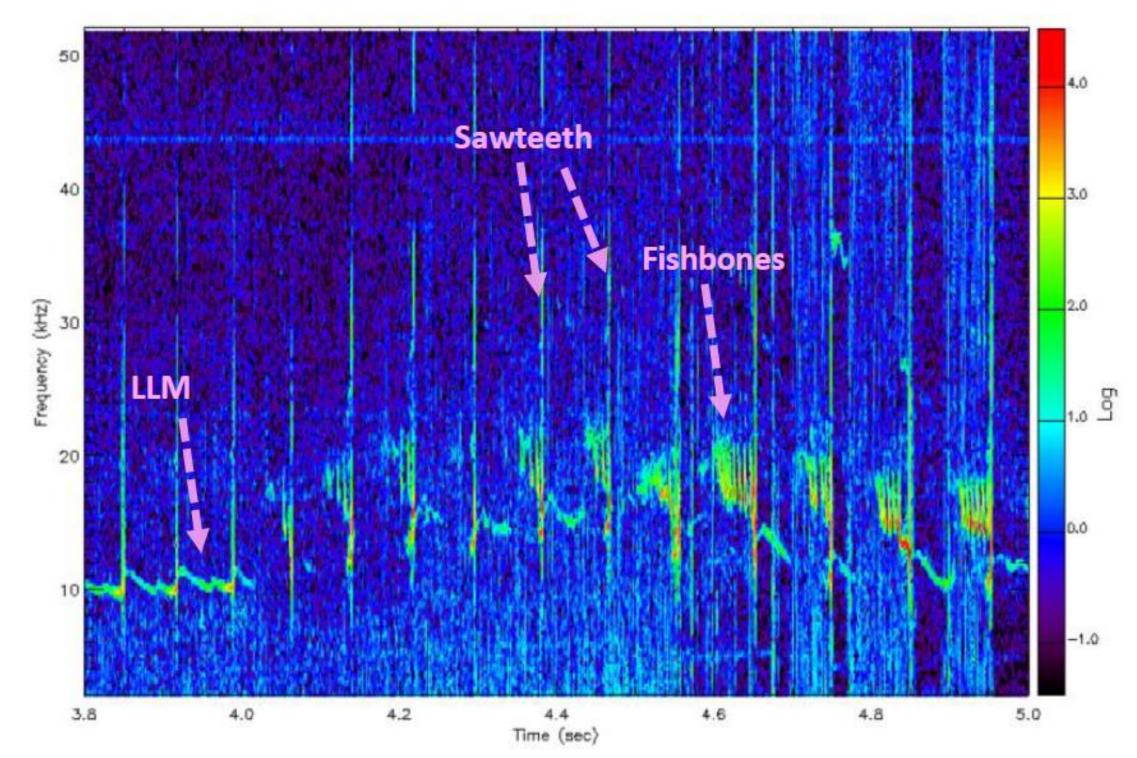


# Physics of the (1,1) (q=1) mode

At large  $I_p$ , as current diffuses inward, it accumulates in the core and q eventually drops below 1. MHD modes appear:

- Internal kink (aka, Long Lived Mode (LLM))
- Sawteeth (reconnection mode)
- Fishbones (fast particle mode)

### **INTRODUCTION TO THE INTERNAL KINK AND THE SAWTOOTH**



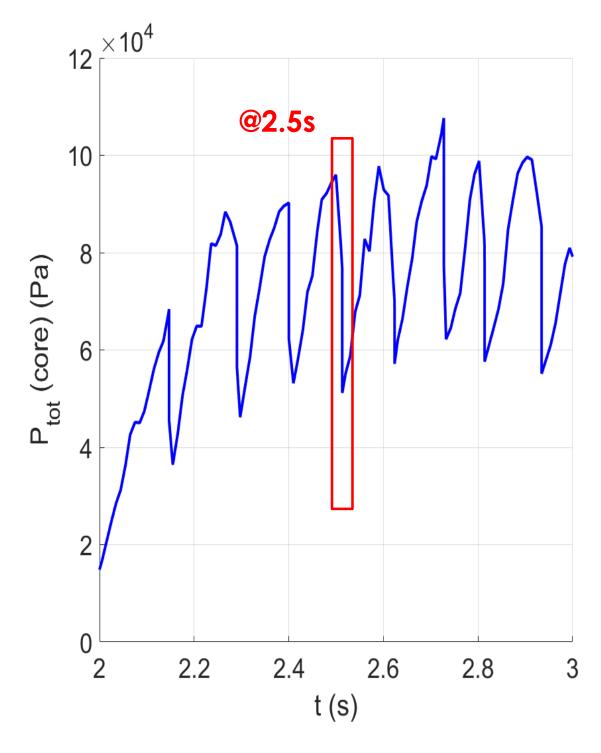
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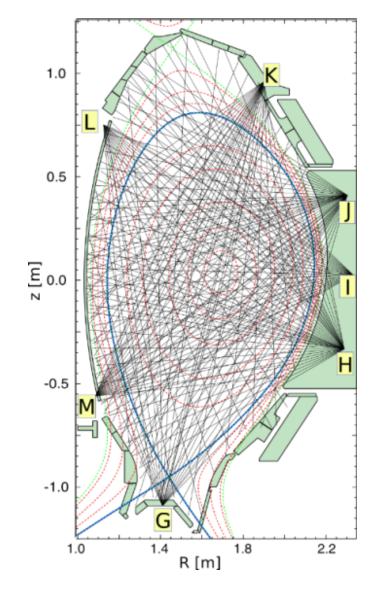






## Experimental measurements with Soft X-ray (SXR) tomography of kink followed by sawtooth crash

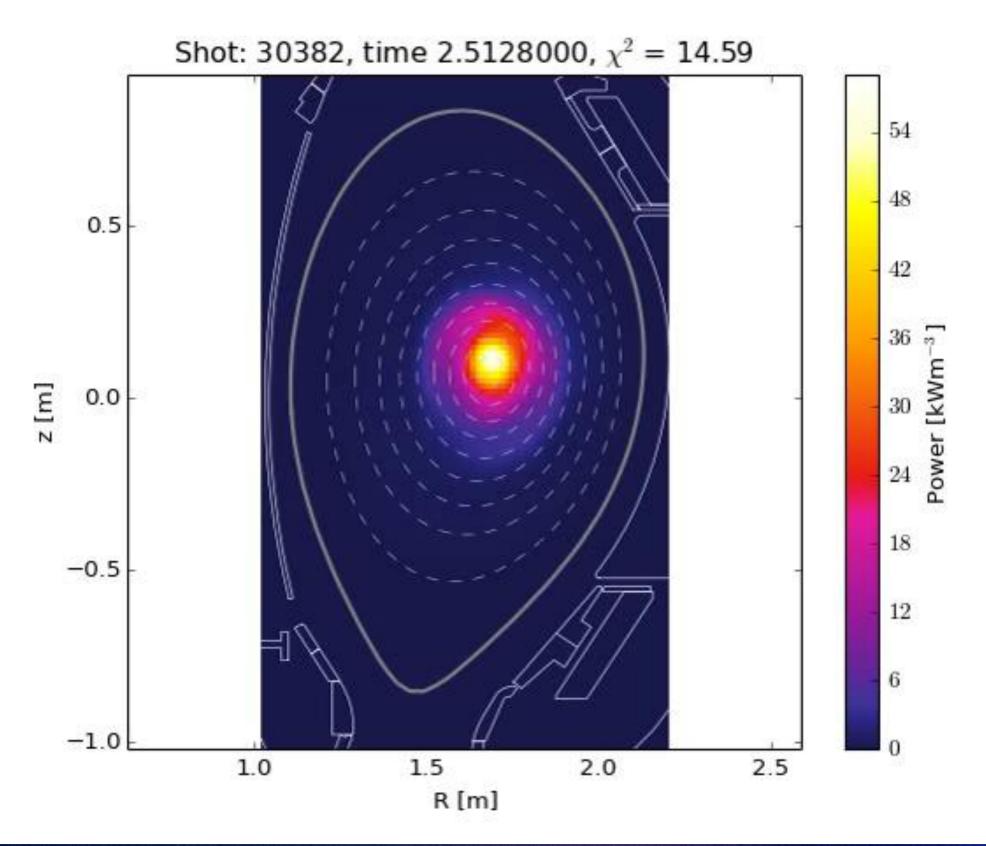




SXR array in ASDEX Upgrade

(AUG#30382@2.5s)

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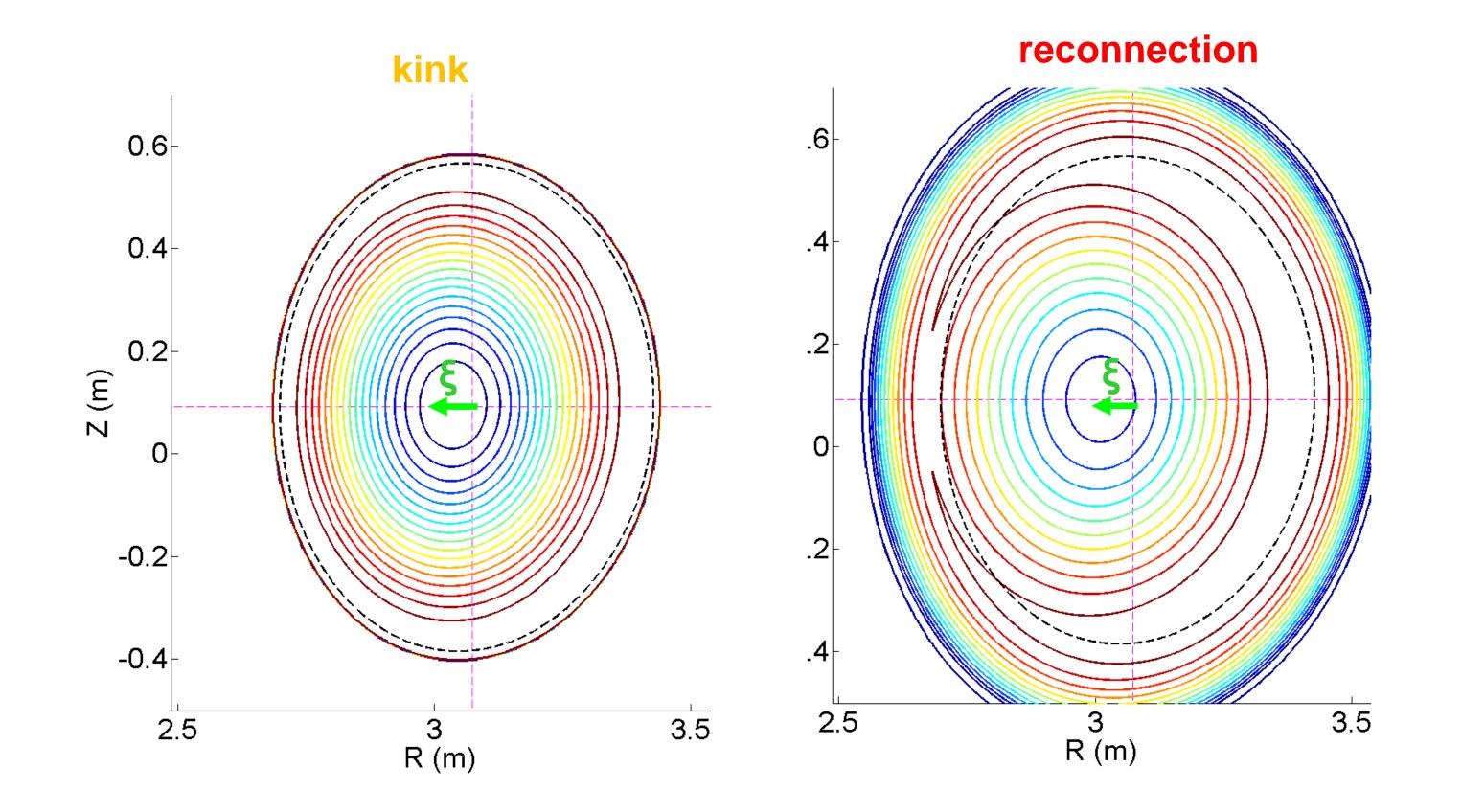








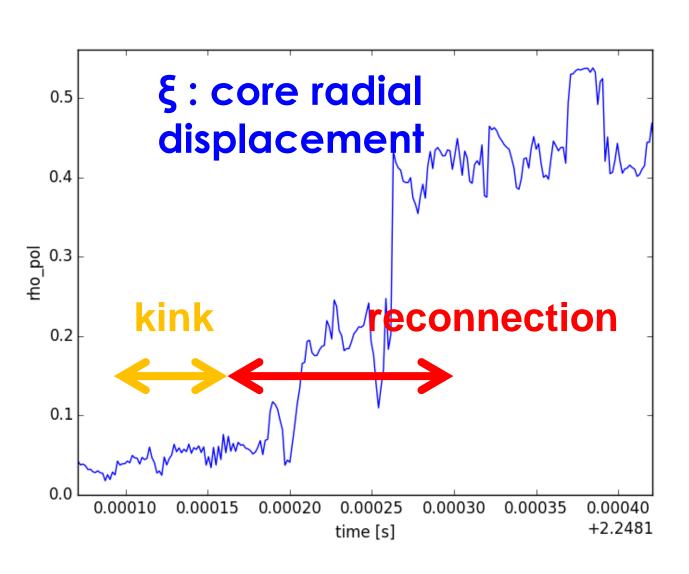
## Patterns of $\psi_*$



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### **INTRODUCTION TO THE INTERNAL KINK AND THE SAWTOOTH**

Ψ**(r,ω)** ω=θ-φ

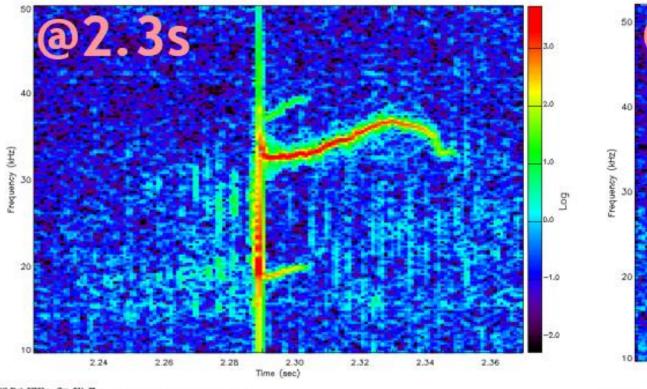








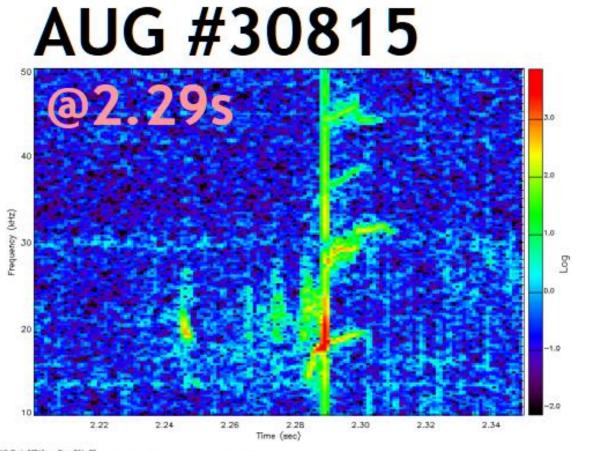
## AUG #30382

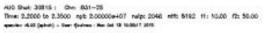


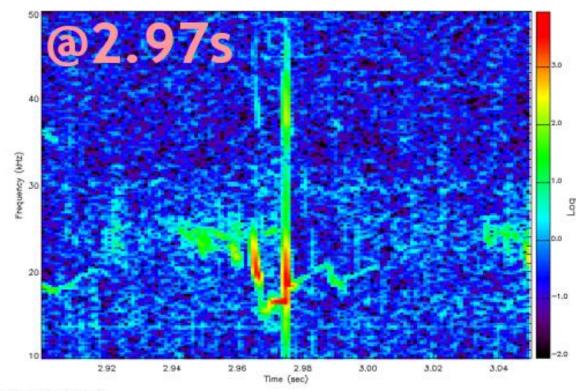
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2.48

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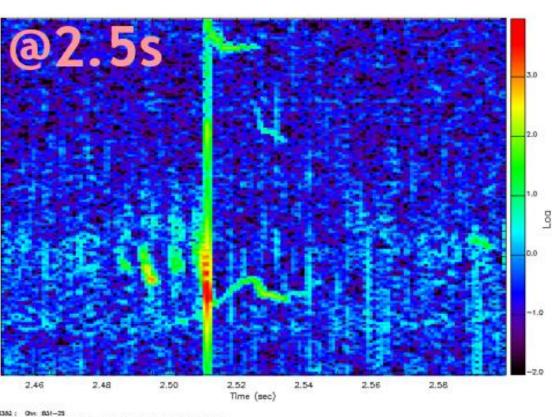


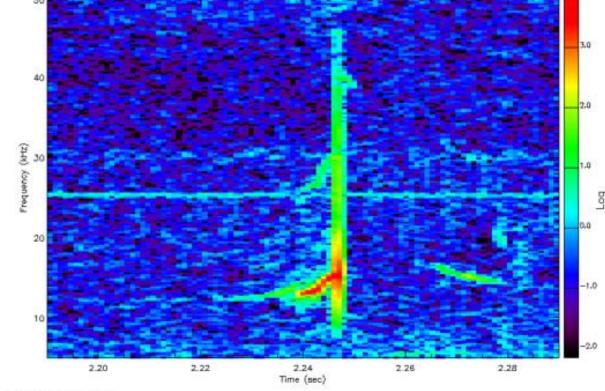
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### **DIVERSITY OF SAWTEETH**







AUS Shuk 31557 : Ohn 631-25 Time 2.1800 to 2.3900 rpt 2.00000+07 nutp: 2048 mitt: 5192 11: 5.000 f2: 50.00 gender 4.65 (shuk) - ber (subse: 51 54 51 158-36 5215

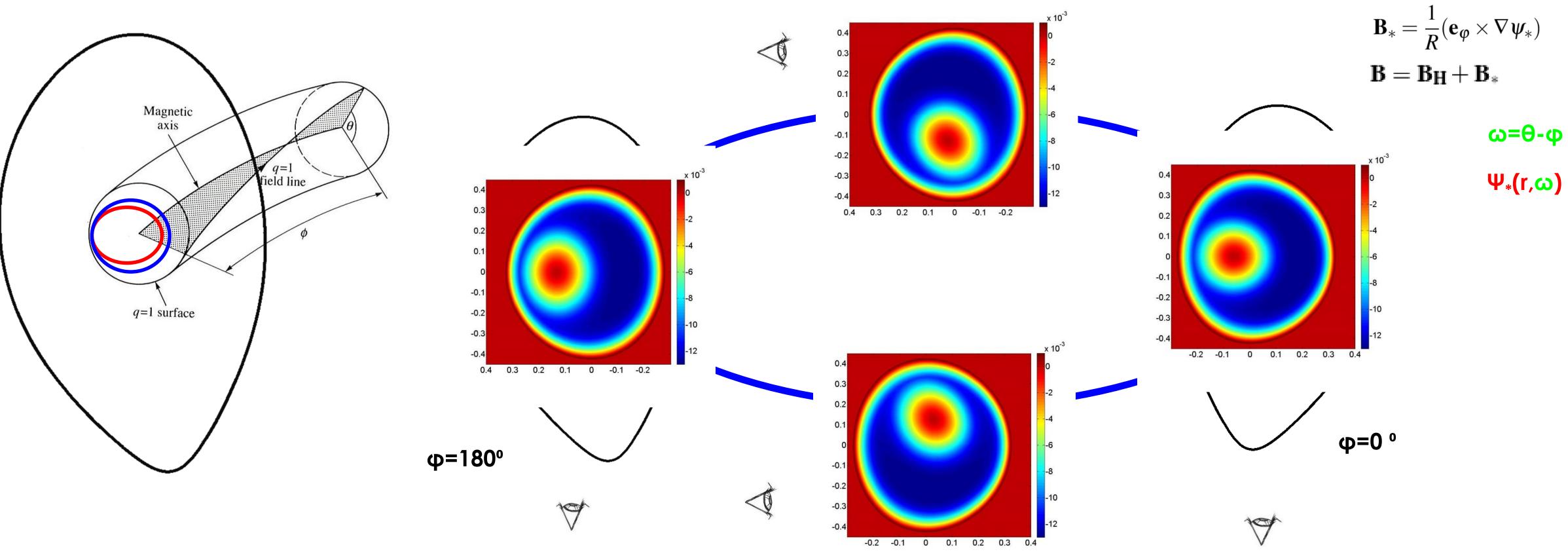




AUS Shot 30380 : One 8034-25 Time: 2,4500 to 2,6000 opt 2,00000+67 nelp: 2048 with: \$192 H1: 10,00 K2: 52,00 queder: 4:48 (phot) - Ber Subnet: Bel In 86 155610 2015



## **STRUCTURE OF PERTURBED HELICAL FLUX**



φ=90 °

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### **INTRODUCTION TO THE INTERNAL KINK AND THE SAWTOOTH**



F. Jaulmes et. al. 2014 Nucl. Fusion 54 104013







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### **ENERGY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**







### MHD : fluid model of plasma

Momentum equation applied to a fluid element moving along the vector  $\xi$  with velocity –i $\xi$  from initial equilibrium:

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho (\mathbf{u} \cdot \nabla) \mathbf{u} = \mathbf{F}(\boldsymbol{\xi}) = -\boldsymbol{\nabla} P + \mathbf{j} \times \mathbf{B}$$

This corresponds to the change of potential energy:

$$\delta W = -\frac{1}{2} \int \left( \mathbf{F}(\boldsymbol{\xi}) \cdot \boldsymbol{\xi}^* \right) d\mathcal{V} \qquad \boldsymbol{\xi}^* \text{ denotes the con}$$



### **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

 $\mathbf{u} = \mathrm{d}\boldsymbol{\xi}/\mathrm{d}t$ 

njugate of the complex displacement vector  $\boldsymbol{\xi}$ .







### MHD : fluid model of plasma

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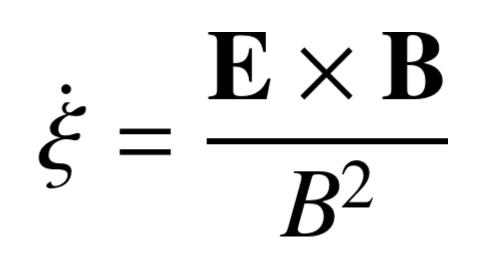
$$\delta W = -\frac{1}{2} \int \left( \mathbf{F}(\boldsymbol{\xi}) \cdot \boldsymbol{\xi}^* \right) \mathrm{d} \mathcal{V} \qquad \boldsymbol{\xi}^* \text{ denotes the con}$$

Conservation of the total energy of the plasma yields:

### **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

 $\mathbf{u} = \mathrm{d}\boldsymbol{\xi}/\mathrm{d}t$ 

njugate of the complex displacement vector  $\boldsymbol{\xi}$ .



W<0 yields destabilization









### MHD : fluid model of plasma

Momentum equation applied to a fluid element moving along the vector  $\xi$  with velocity –i $\xi$  from initial equilibrium:

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho (\mathbf{u} \cdot \nabla) \mathbf{u} = \mathbf{F}(\boldsymbol{\xi}) = -\boldsymbol{\nabla} P + \mathbf{j} \times \mathbf{B}$$

This corresponds to the change of potential energy:

$$\delta W = -\frac{1}{2} \int \left( \mathbf{F}(\boldsymbol{\xi}) \cdot \boldsymbol{\xi}^* \right) \mathrm{d} \mathcal{V} \qquad \boldsymbol{\xi}^* \text{ denotes the con}$$

Expressing as a function of perturbed magnetic field:  $\mathbf{B_1} = \nabla \times (\boldsymbol{\xi}_{\perp} \times \mathbf{B})$   $\mu_0 \mathbf{j} = \nabla \times \mathbf{B}$ 

$$\begin{split} \delta W &= \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_1^2}{\mu_0} + \frac{B^2}{\mu_0} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} | \\ \text{Plasma only!} \\ &- 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B_1} \cdot \\ &+ \gamma_{\text{thermo}} P(\boldsymbol{\nabla} \cdot \boldsymbol{\xi})^2 \right] \mathrm{d}\mathcal{V} \end{split}$$

### **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

 $\mathbf{u} = \mathrm{d}\boldsymbol{\xi}/\mathrm{d}t$ 

njugate of the complex displacement vector  $\boldsymbol{\xi}$ .

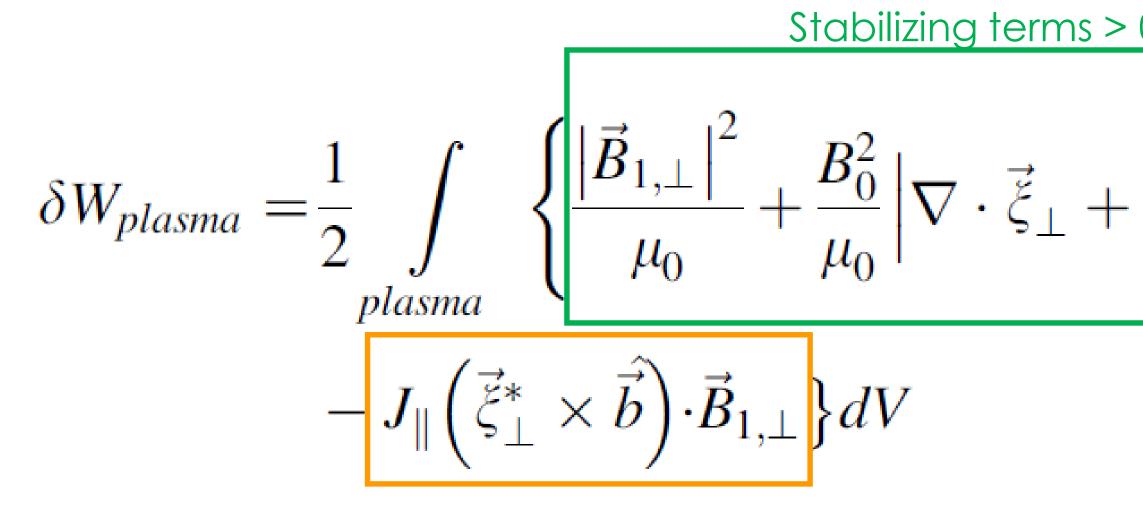
|2|

 $(\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel}$ 





## Discussion on plasma stability term in energy principle



Possibly destabilizing term

Thorough study needs to include also vacuum region and stabilizing effect of the conductive wall.... Book: Active Control of Magnetohydrodynamic Instabilities in Hot Plasmas - Valentin Igochine

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## **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

$$+2\vec{\xi}_{\perp}\cdot\vec{\kappa}\Big|^{2}+\Gamma p_{0}\Big|\nabla\cdot\vec{\xi}\Big|^{2}-2\Big(\vec{\xi}_{\perp}\cdot\nabla p_{0}\Big)\Big(\vec{\kappa}\cdot\vec{\xi}_{\perp}^{*}\Big)$$

Possibly destabilizing term









Change of potential energy:

$$\delta W = \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_1^2}{\mu_0} + \frac{B^2}{\mu_0} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^2 - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi}) - 2(\boldsymbol{\xi} \cdot \boldsymbol{\xi} \cdot \boldsymbol{\xi}$$

 $\mathbf{B_1} = \nabla \times (\boldsymbol{\xi}_{\perp} \times \mathbf{B})$ 

$$\omega^2 = \frac{2\delta W}{\int \rho_i |\boldsymbol{\xi}_0|^2 \mathrm{d}\mathcal{V}} \delta W_{m=1} = \pi^2 \frac{B_0^2}{R_0} \int_0^a r^3 |\boldsymbol{\xi}_r'|^2 \left(1 - \frac{1}{q}\right)^2 dr$$

$$\gamma_I^2 = -\omega^2$$
 Plugging .....

• • • • • • • • • • •

### **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

Considering an approximate circular geometry (nealecting toroidal displacement)

always stabilizing for  $m \geq 2$  modes

in the observed radial shape of the displacement function.....

.....and doing lots of tedious algebra.....

$$\xi_{in} = \xi_0 \left[ 1 - \frac{2}{\pi} \arctan\left( x \frac{B_{0\varphi}}{\sqrt{3\rho\mu_0}R_0} \frac{s_1}{\gamma_I} \right) \right] \quad \text{with} \quad x = 1 -$$









Change of potential energy:

$$\delta W = \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_1^2}{\mu_0} + \frac{B^2}{\mu_0} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^2 - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} + \gamma_{\text{thermo}} P(\boldsymbol{\nabla} \cdot \boldsymbol{\xi})^2 \right] d\mathcal{V}$$

$$\mathbf{B_1} = \nabla \times (\boldsymbol{\xi}_{\perp} \times \mathbf{B})$$

$$\omega^2 = \frac{2\delta W}{\int \rho_i |\boldsymbol{\xi}_0|^2 \mathrm{d} \mathcal{V}}$$
$$\gamma_I^2 = -\omega^2$$



### **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

We find an ideal stability criteria mostly based on the poloidal beta inside q=1

$$\beta_p(r_1) \equiv -2 \frac{R_0^2 q^2}{B_0^2 r_1^4} \int_0^{r_1} p' r^2 dr \,.$$

This quantity represents the total available kinetic energy within  $r = r_1$ . A simple form for  $\delta W$  can be obtained if we consider a parabolic current profile  $j_{\phi}(r)$ , and if we assume that q(r) in the centre does not differ very much from unity,

$$|1 - q(0)| \ll 1$$
,  $q(0) < 1$ .

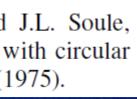
Then, the m = 1 internal kink mode is mainly pressure driven and the potential energy is approximately [18]

$$\delta W \approx 6\pi^2 \frac{B_0^2 r_1^4}{R_0^3} |\xi_r(0)|^2 \left[1 - q(0)\right] \left[\beta_{\rm crit}^2 - \beta_p^2(r_1)\right],$$
(27)

where  $\beta_{\text{crit}}^2 = \frac{13}{144}$ . One sees that instability,  $\delta W < 0$ , occurs if the driving force  $\beta_p$  exceeds the threshold value  $\beta_{\rm crit} \approx$ 0.3.

> 18. M.N. Bussac, R. Pellat, D. Edery, and J.L. Soule, "Internal kink modes in toroidal plasma with circular cross-section," Phys. Rev. Lett. 35, 1638 (1975).





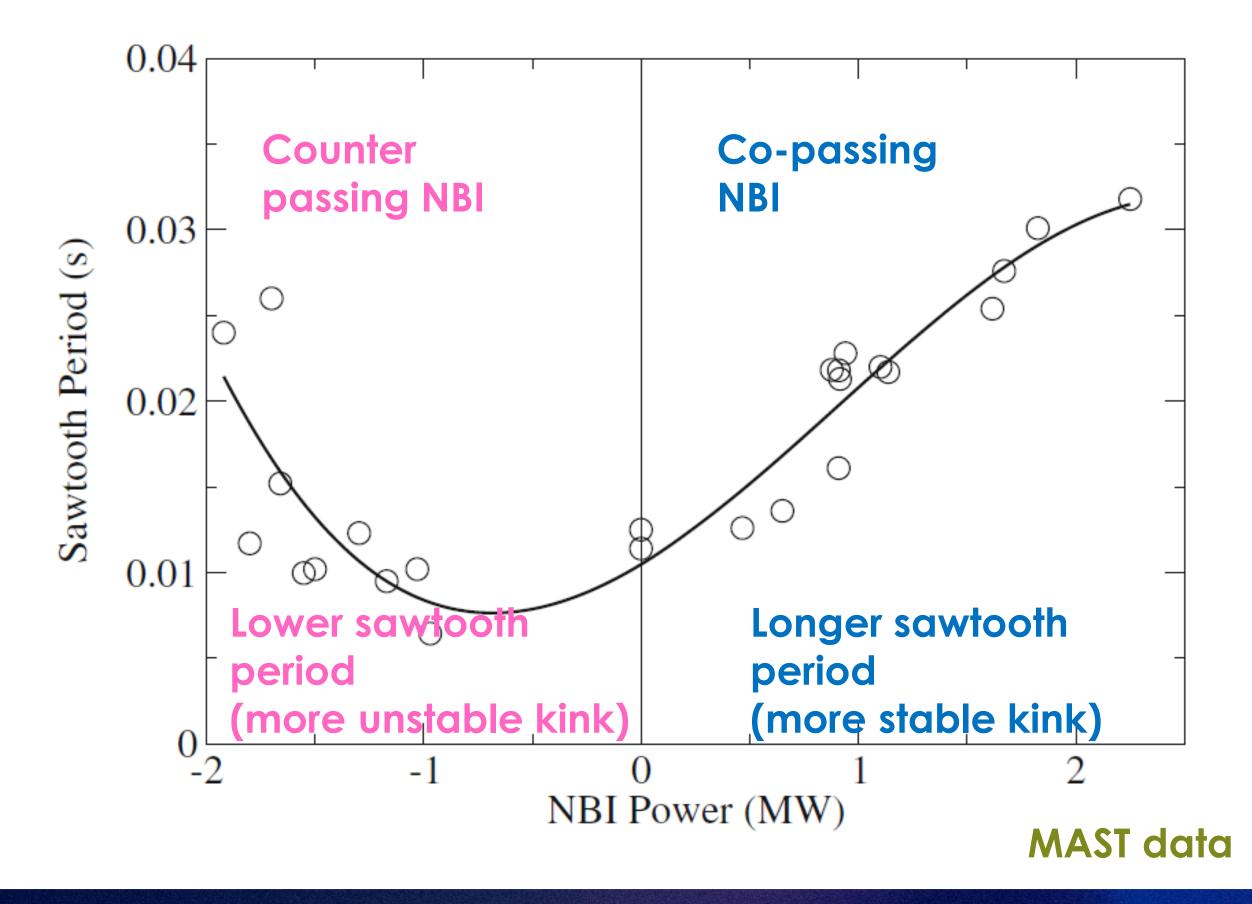


# Illustration of the energy principle to explain experimental effect of stabilization of kink by NBI particles

$$\begin{split} \delta W &= \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_{1}^{2}}{\mu_{0}} + \frac{B^{2}}{\mu_{0}} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^{2} \right. \\ &\left. - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^{*}) - \mathbf{B}_{1} \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} \right. \\ &\left. + \gamma_{\text{thermo}} P(\boldsymbol{\nabla} \cdot \boldsymbol{\xi})^{2} \right] \mathrm{d} \mathcal{V} \end{split}$$



## GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK







## Illustration of the energy principle to explain experimental effect of stabilization of kink by NBI particles

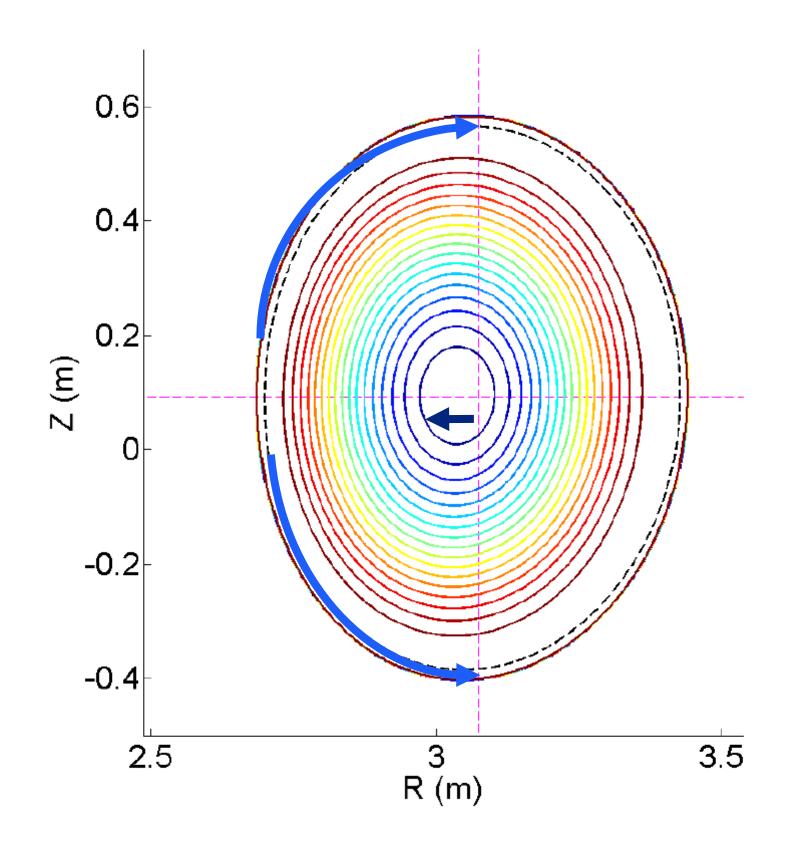
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$$\boldsymbol{\xi} = \int \boldsymbol{\dot{\xi}} \mathrm{d}t \simeq \mathbf{v_E} \, \mathrm{d}t \; .$$

$$\delta W_{\text{fast}} = -\int_0^{r_1} \left( \boldsymbol{\xi} \cdot \nabla P_{\text{fast}} \right) \left( \boldsymbol{\xi} \cdot \boldsymbol{\kappa} \right) \mathrm{d} \boldsymbol{\mathcal{V}}$$

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## **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**



The backflow of plasma is always tangential to the q=1 contour! (at any toroidal location)









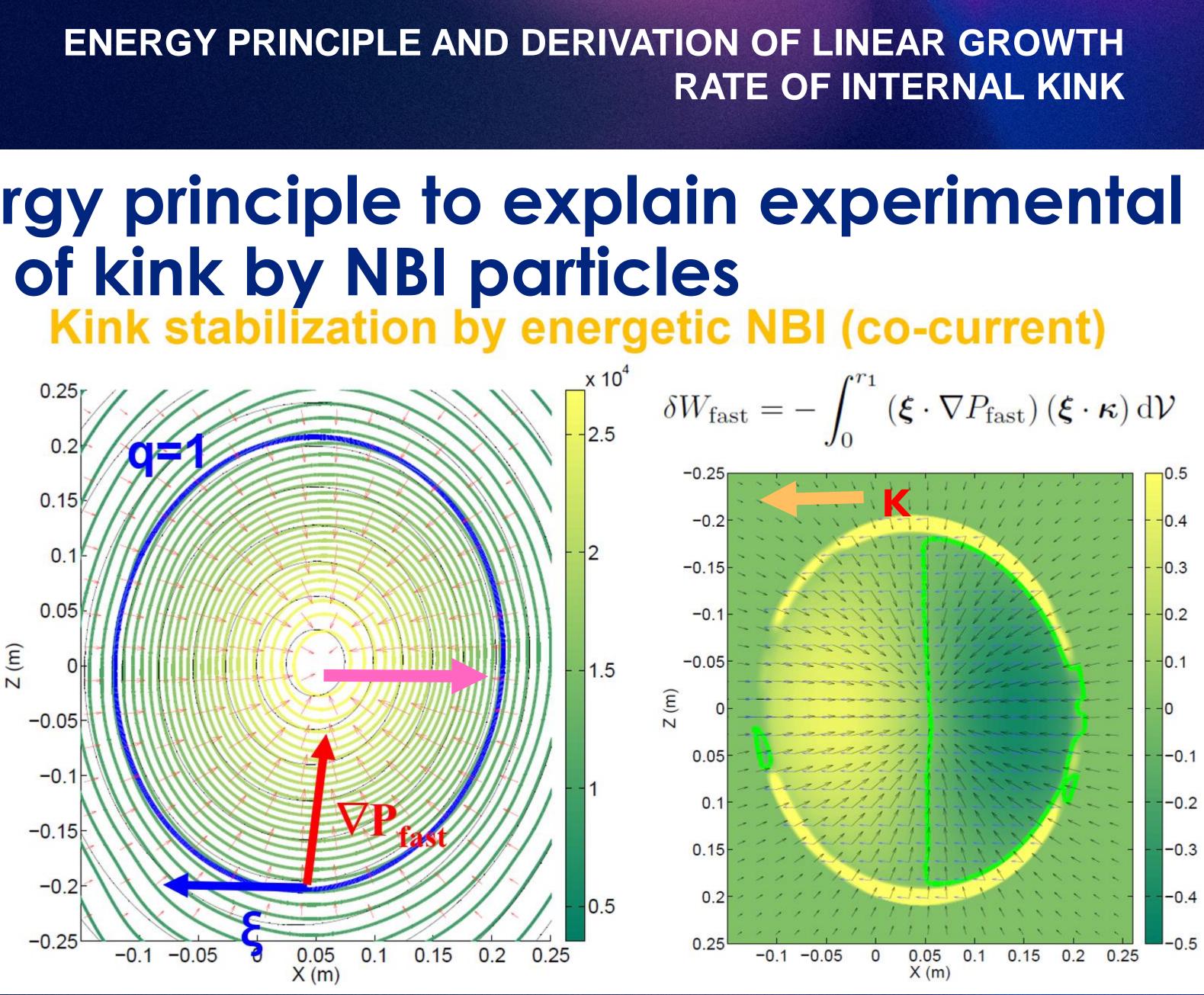
# Illustration of the energy principle to explain experimental effect of stabilization of kink by NBI particles Kink stabilization by energetic NBI (co-current)

$$\delta W_{\text{fast}} = -\int_0^{r_1} \left( \boldsymbol{\xi} \cdot \nabla P_{\text{fast}} \right) \left( \boldsymbol{\xi} \cdot \boldsymbol{\kappa} \right) \mathrm{d} \boldsymbol{\mathcal{V}}$$

$$P_{\text{fast}} = (2/3) n_{\text{fast}} \langle \mathcal{E}_{\text{fast}} \rangle$$

$$\boldsymbol{\kappa_{pol}} = \frac{\mu_0}{B^2} \boldsymbol{\nabla} \left( P + \frac{B^2}{2\mu_0} \right) ;$$
  
$$\boldsymbol{\kappa_{\varphi}} = \left( \frac{(\mathbf{B} \times \boldsymbol{\nabla} B) \times \mathbf{B}}{B^3} \right)_{\varphi} .$$

$$\boldsymbol{\xi} = \int \boldsymbol{\dot{\xi}} \mathrm{d}t \simeq \mathbf{v}_{\mathbf{E}} \, \mathrm{d}t$$



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## Illustration of the energy principle to explain experimental effect of stabilization of kink by NBI particles Kink destabilization by energetic NBI (counter-current)

Z (m)

-0.05

-0

-0.15

-0.2

-0.25

$$\delta W = \frac{1}{2} \int_{\mathcal{V}} \begin{bmatrix} \frac{B_1^2}{\mu_0} + \frac{B^2}{\mu_0} |\nabla \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa}|^2 & 0.25 \\ -2(\boldsymbol{\xi}_{\perp} \cdot \nabla P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b})j_{\parallel} & 0.15 \\ +\gamma_{\text{thermo}} P(\nabla \cdot \boldsymbol{\xi})^2 \end{bmatrix} d\mathcal{V} & 0.15 \\$$

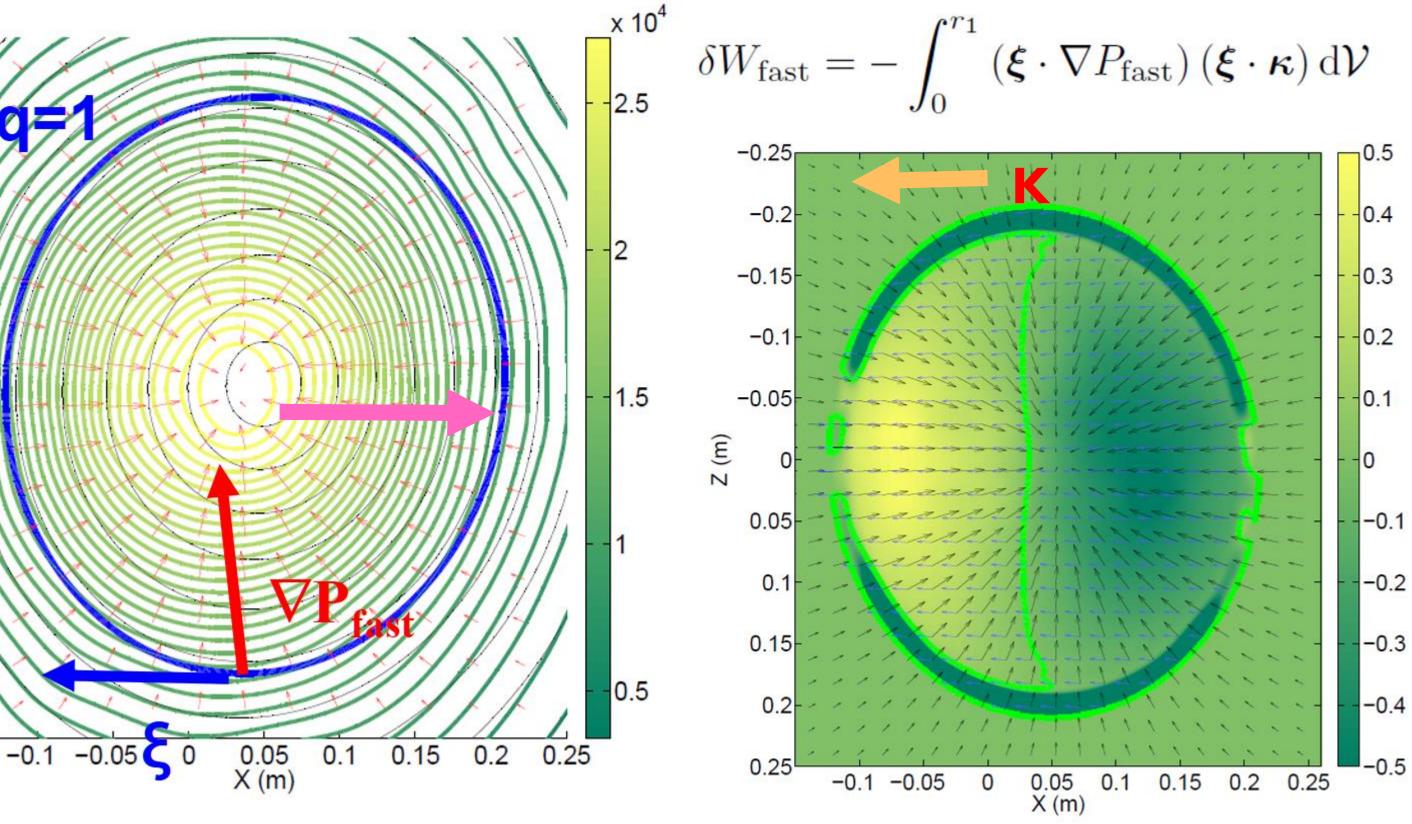
$$P_{\text{fast}} = (2/3) n_{\text{fast}} \langle \mathcal{E}_{\text{fast}} \rangle$$

$$\boldsymbol{\kappa_{pol}} = \frac{\mu_0}{B^2} \boldsymbol{\nabla} \left( P + \frac{B^2}{2\mu_0} \right) ;$$
  
$$\boldsymbol{\kappa_{\varphi}} = \left( \frac{(\mathbf{B} \times \boldsymbol{\nabla} B) \times \mathbf{B}}{B^3} \right)_{\varphi} .$$

$$\boldsymbol{\xi} = \int \boldsymbol{\dot{\xi}} \mathrm{d}t \simeq \mathbf{v}_{\mathbf{E}} \, \mathrm{d}t \; .$$

25.04.2023

## ENERGY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK







# **Overview of this lecture**

- Safety factor profile in tokamaks
- Introduction to the internal kink and the sawtooth crash
- Energy principle and derivation of linear growth rate of internal kink
- Ideal MHD for poloidal mapping of the reconnecting magnetic flux
- Computationally efficient poloidal mapping of the reconnecting magnetic flux

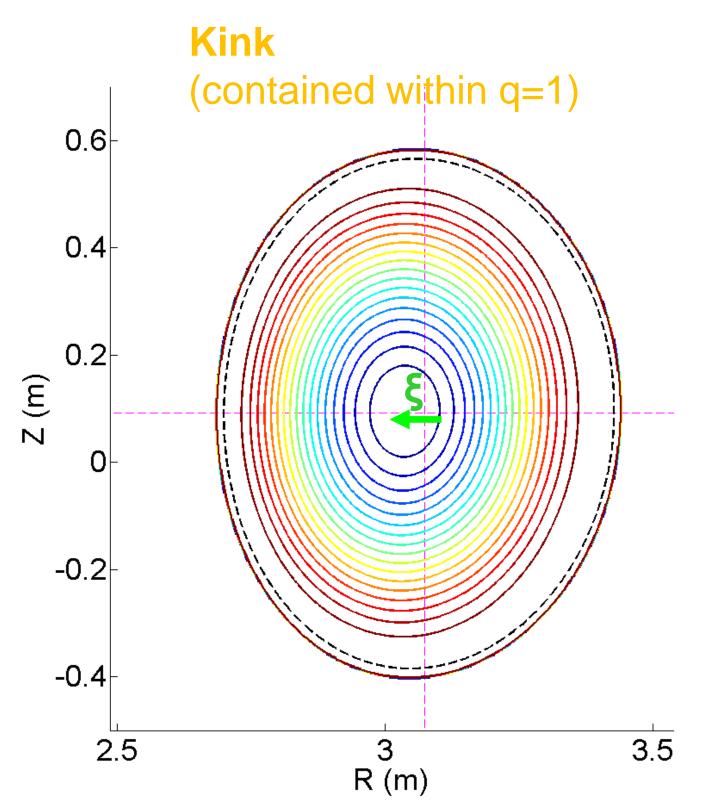
## **INTRODUCTION TO INTERNAL KINK AND SAWTOOTH**





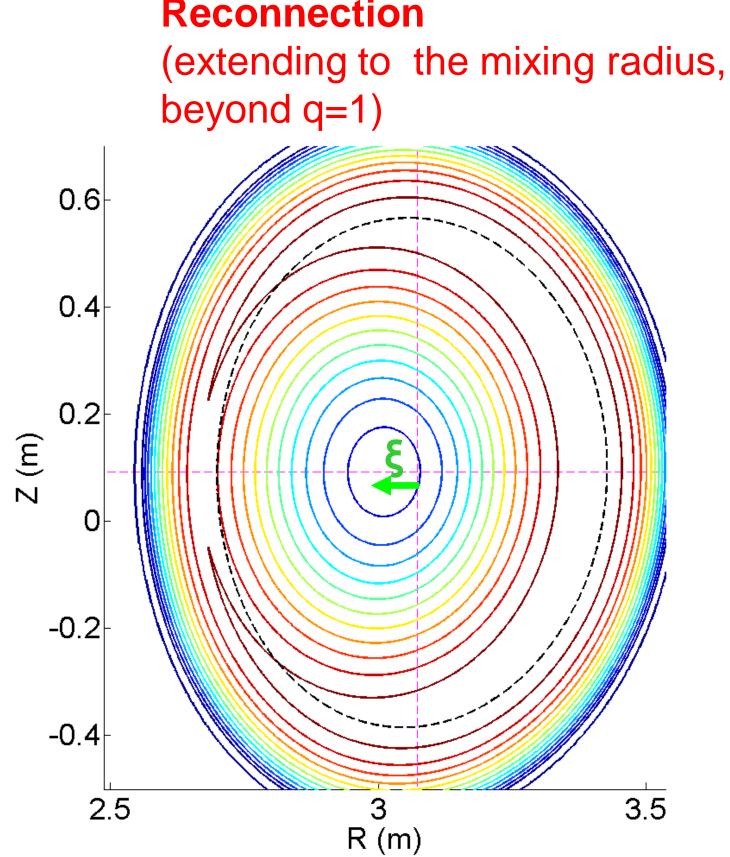


# Poloidal flux contour of the internal kink and sawtooth reconnection



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### **INTRODUCTION TO TOKAMAKS**

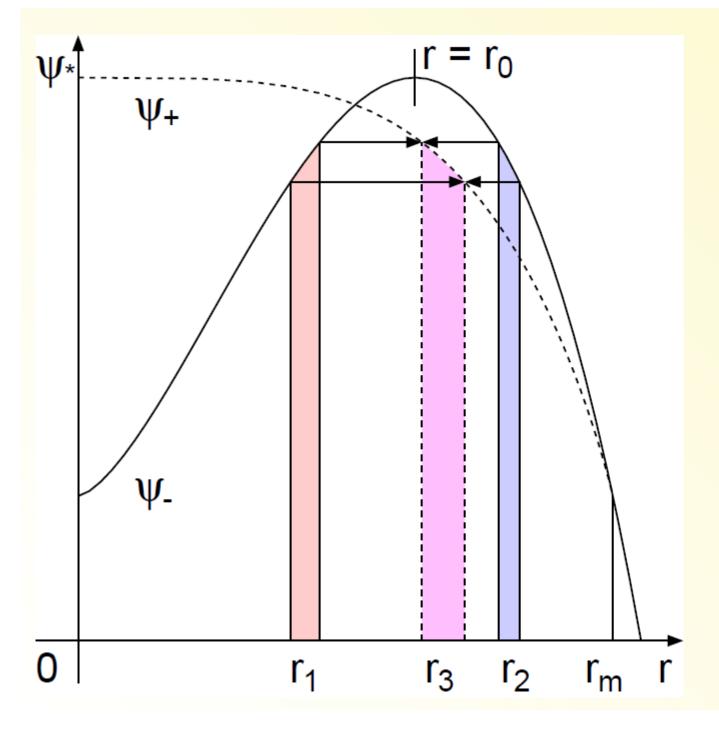








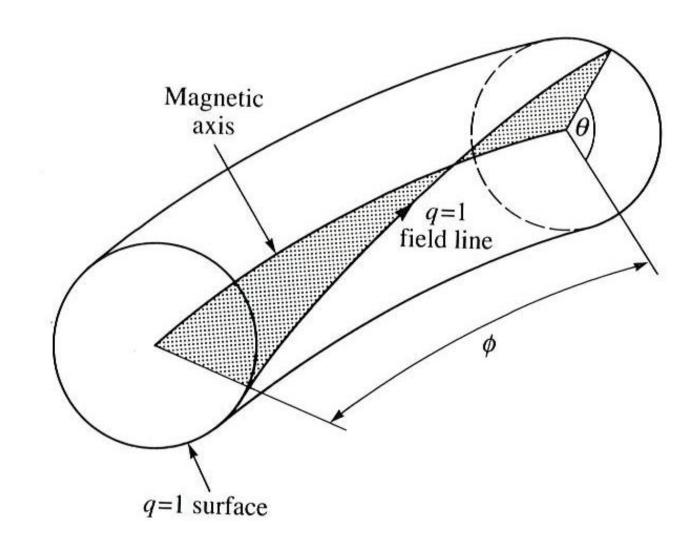
## The perturbed helical flux



Initial  $(\psi_{-})$  and final  $(\psi_{+})$  helical flux profiles as a function of The arrows indicate the conr. servation of helical flux during reconnection, while conservation of toroidal flux is given by  $r_2^2 - r_1^2 =$  $r_{3}^{2}$ .

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### **INTRODUCTION TO TOKAMAKS**



Ψ**(r,ω)** ω=θ-φ

 $\mathbf{B}_{\mathbf{H}} = \mathbf{B}_{\varphi} + q \mathbf{B}_{\mathbf{pol}}$  $\mathbf{B}_* = \frac{1}{R} (\mathbf{e}_{\varphi} \times \nabla \psi_*)$ 

$$\mathbf{B} = \mathbf{B}_{\mathbf{H}} + \mathbf{B}_{*}$$

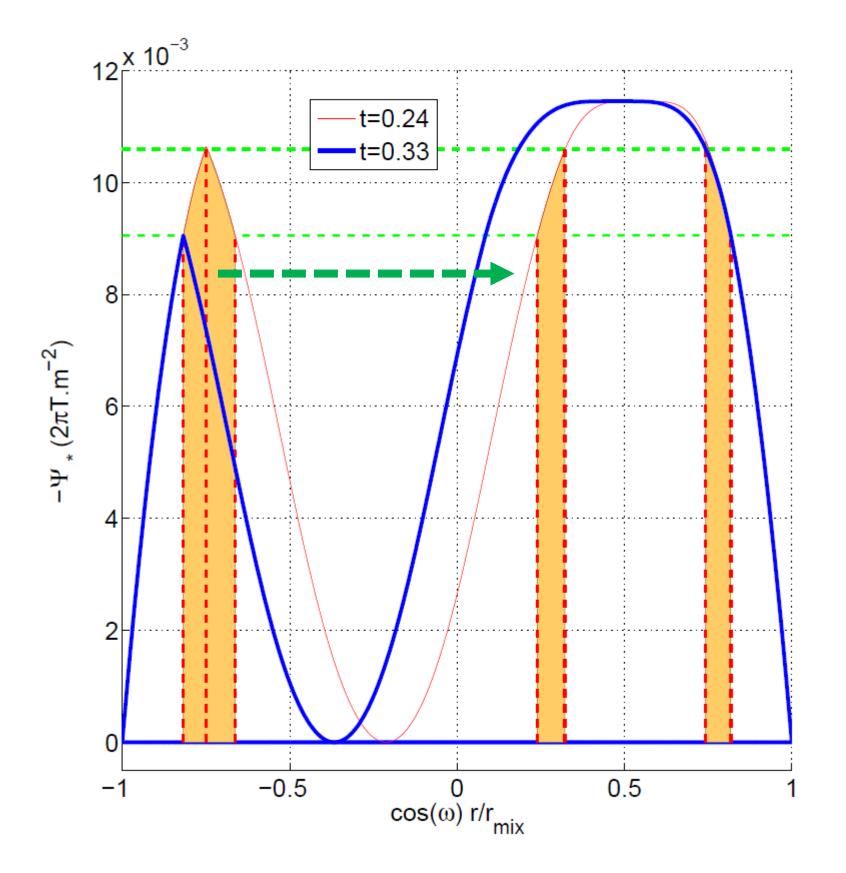






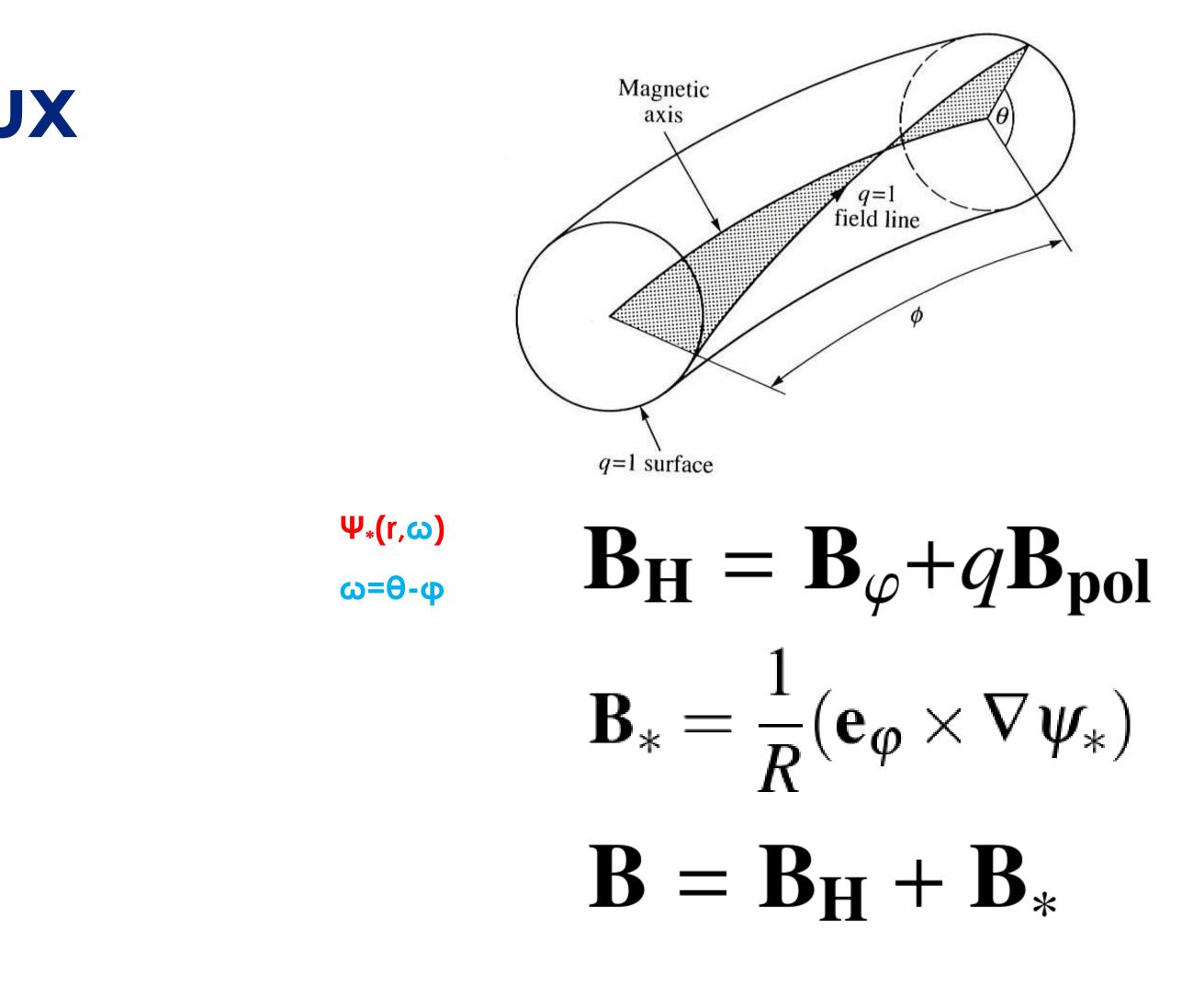


## The perturbed helical flux



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### **INTRODUCTION TO TOKAMAKS**









## **MHD** model

### Ideal MHD : fluid model of plasma

The mass continuity equation is

$$rac{\partial
ho}{\partial t}+
abla\cdot\left(
ho{f v}
ight)=0.$$

The Cauchy momentum equation is

$$ho\left(rac{\partial}{\partial t}+\mathbf{v}\cdot
abla
ight)\mathbf{v}=\mathbf{J} imes\mathbf{B}-
abla p.$$

The Lorentz force term  $\mathbf{J} imes \mathbf{B}$  can be expanded using Ampère's law and the vector calculus identity

$$\frac{1}{2}
abla(\mathbf{B}\cdot\mathbf{B}) = (\mathbf{B}\cdot
abla)\mathbf{B} + \mathbf{B} imes(
abla imes\mathbf{B})$$

to give

$$\mathbf{J} imes \mathbf{B} = rac{\left(\mathbf{B} \cdot 
abla 
ight) \mathbf{B}}{\mu_0} - 
abla \left(rac{B^2}{2\mu_0}
ight),$$

where the first term on the right hand side is the magnetic tension force and the second term is the magnetic pressure force.

The ideal Ohm's law for a plasma is given by  $\mathbf{E} + \mathbf{v} \times \mathbf{B} = 0.$ 

Faraday's law is

$$rac{\partial {f B}}{\partial t} = -
abla imes {f E}.$$

The low-frequency Ampère's law neglects displacement current and is given by

 $\mu_0 \mathbf{J} = \nabla \times \mathbf{B}.$ 

The magnetic divergence constraint is

 $abla \cdot \mathbf{B} = 0.$ 

The energy equation is given by

$$rac{\mathrm{d}}{\mathrm{d}t}\left(rac{p}{
ho^{\gamma}}
ight)=0,$$

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### PARTICLES AND HEAT TRANSPORT

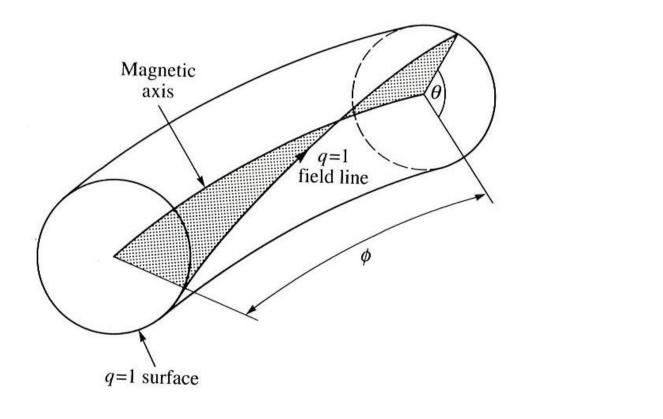
$$\mathbf{E} = -\frac{\partial \mathbf{A}}{\partial t} - \boldsymbol{\nabla} \Phi$$

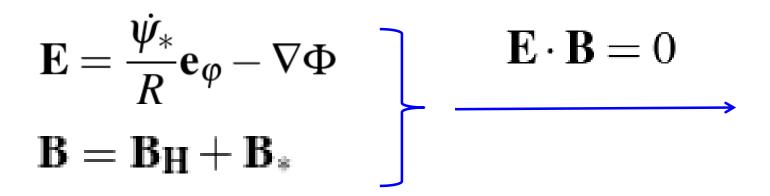






## Simplified poloidal flux modelling of the sawtooth crash





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**INTRODUCTION TO TOKAMAKS** 

 $\mathbf{E} + \mathbf{u} \times \mathbf{B} = \eta \mathbf{j}$ 

Ideal Ohm's law:

## $\mathbf{E} + \mathbf{u} \times \mathbf{B} = 0 \longrightarrow \mathbf{E} \cdot \mathbf{B} = 0$

$$\nabla \Phi \cdot \mathbf{B}_* = \frac{B_{\varphi} \dot{\psi}_*}{R}$$

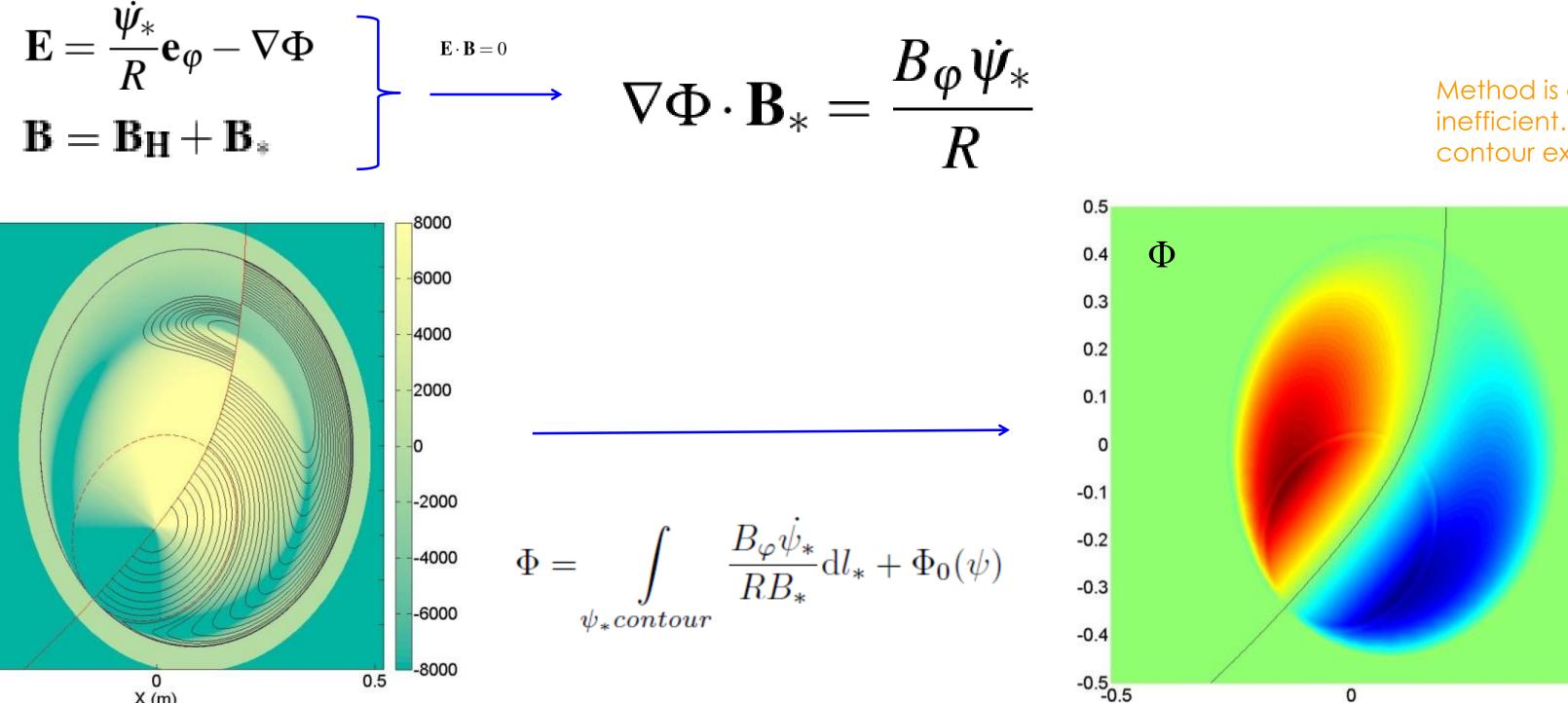


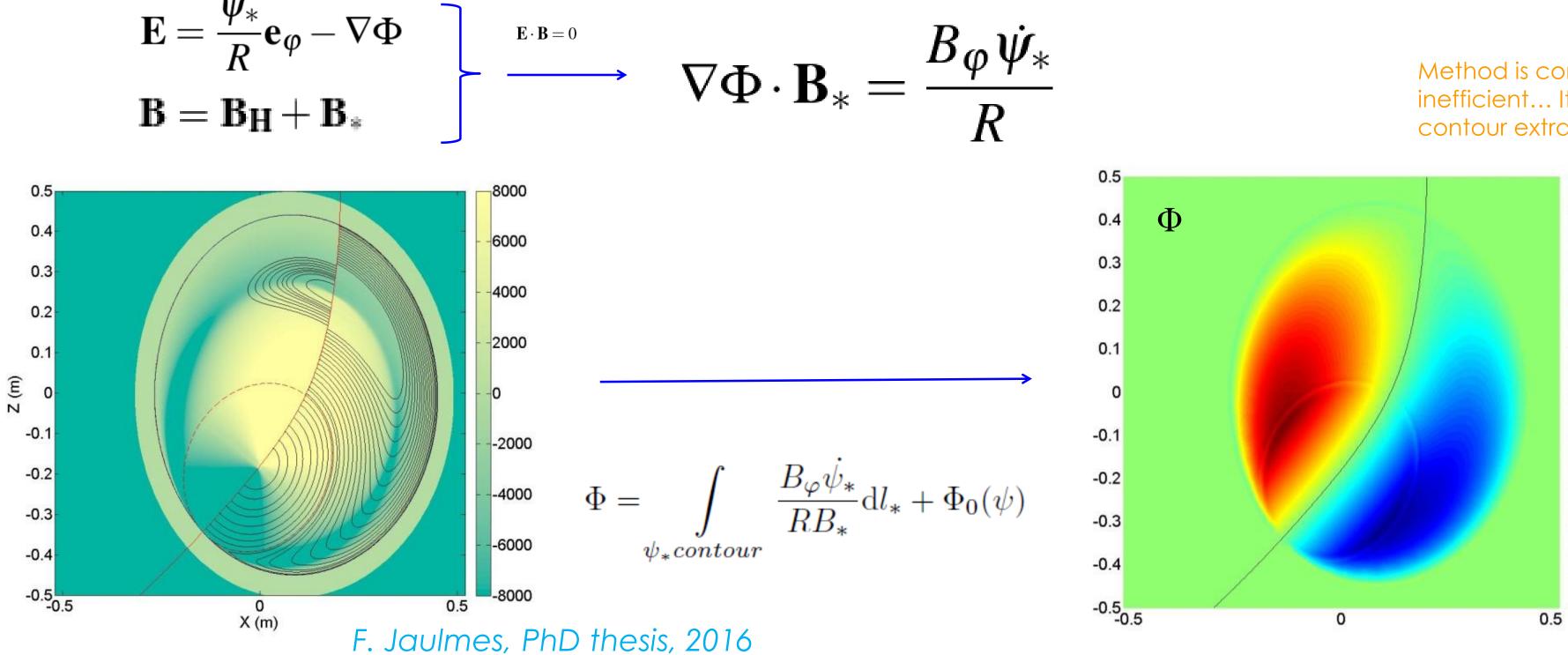


## Simplified poloidal flux modelling of the sawtooth crash

Ya. I. Kolesnichenko et. Al Nucl. Fusion 36 159 (1996)

 $\mathbf{E} \cdot \mathbf{B} = 0$  $\mathbf{E} + \mathbf{u} \times \mathbf{B} = 0$ 





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### **INTRODUCTION TO TOKAMAKS**

Method is computationally inefficient... It requires contour extraction!

2000

1500

1000

500

-500

-1000

-1500

-2000





# **Overview of this lecture**

- Safety factor profile in tokamaks
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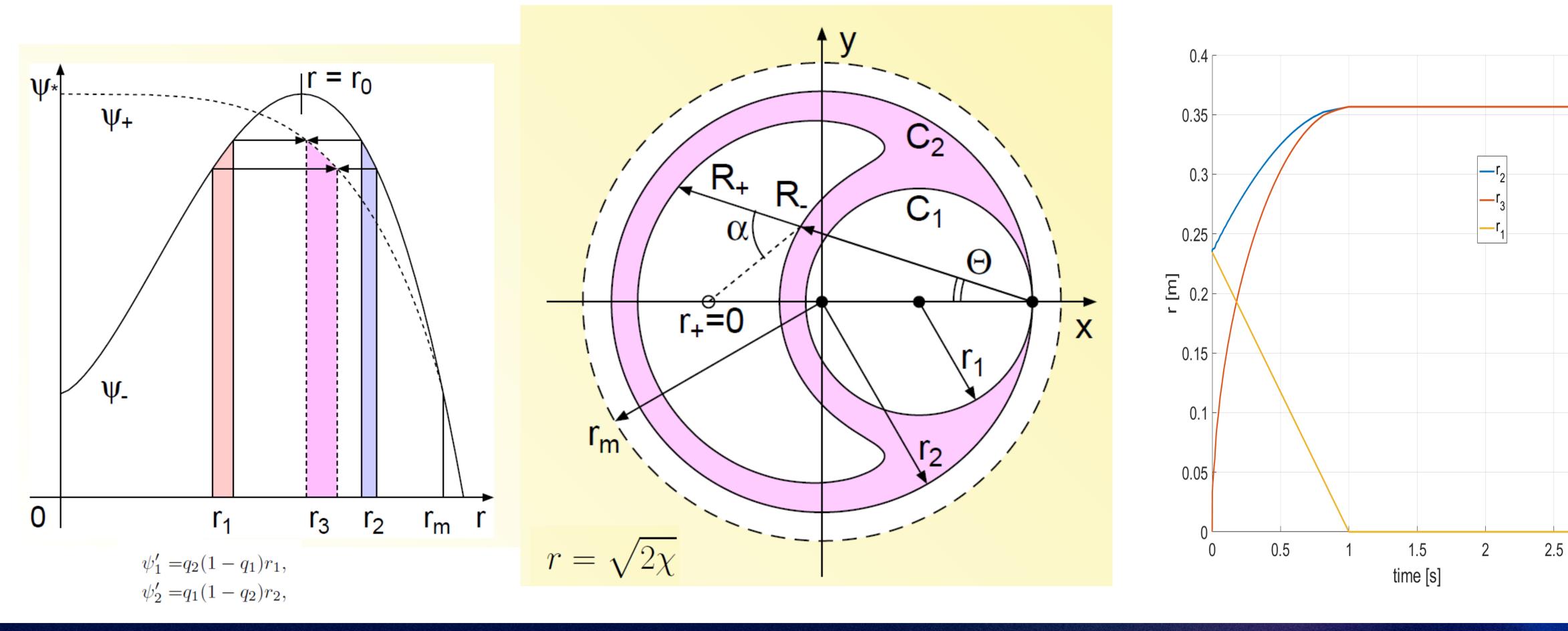
### **INTRODUCTION TO TOKAMAKS**

How to improve the Electric potential calculation?







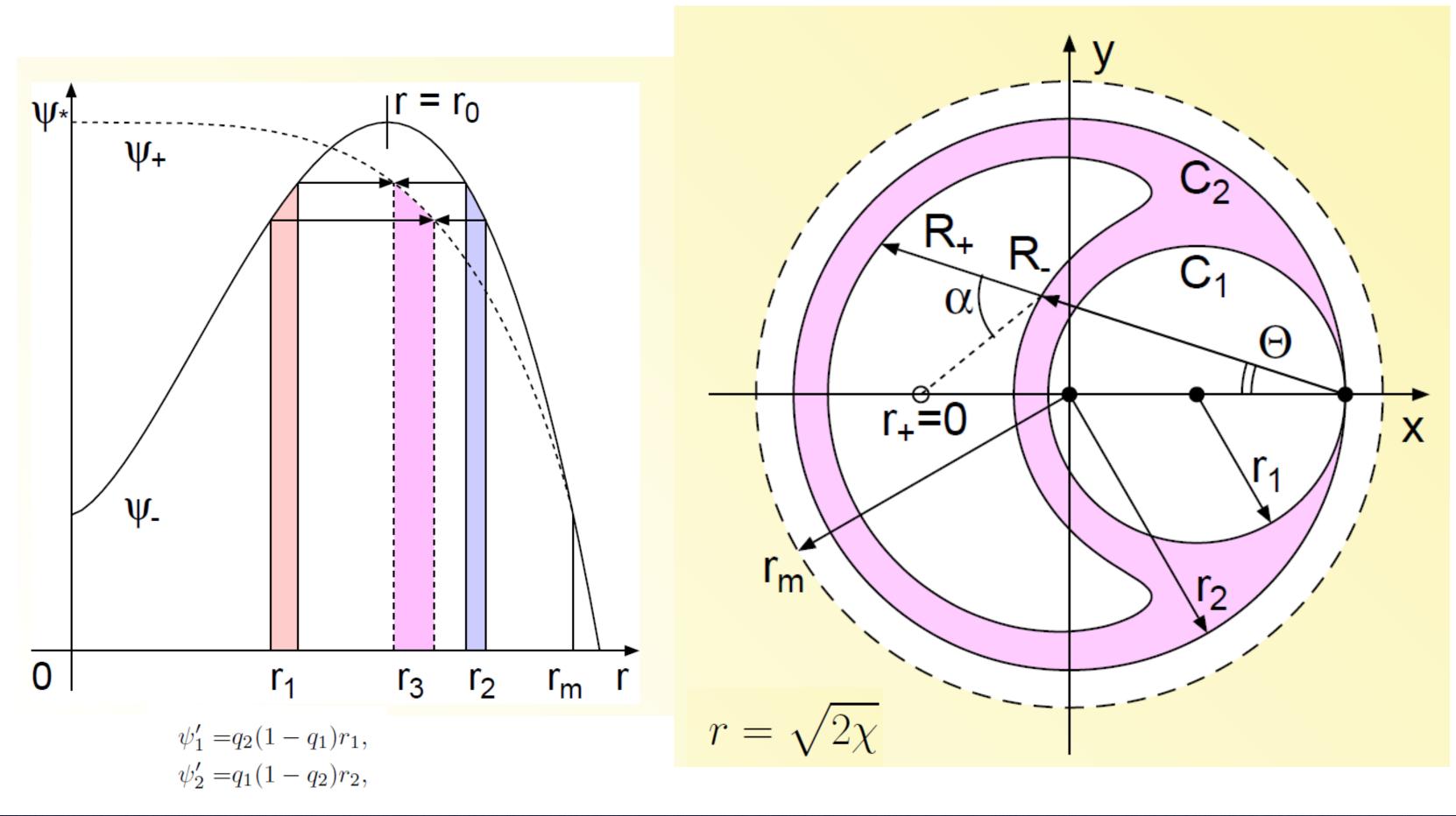


## **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**

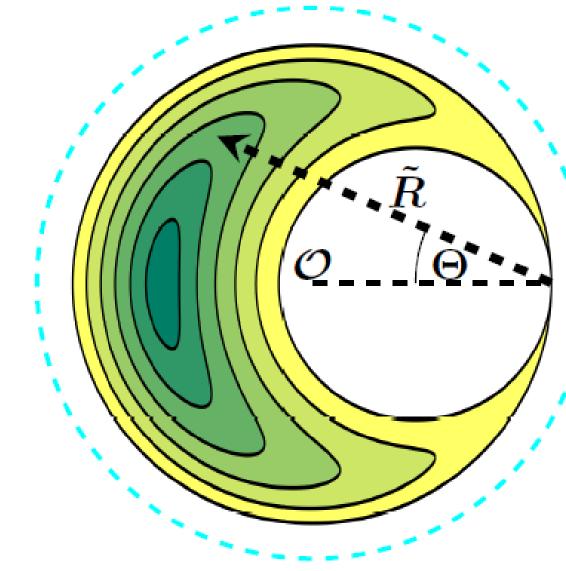






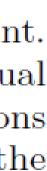


## **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**



Coordinates  $\tilde{R}, \Theta$  defined from the 'X'-point. Contours drawn here indicate surfaces of equal  $r_+$  and enclose an area  $\pi r_+^2$ . Transformations in this model *preserve* this area, thus  $r_+$  is the radial coordinate after the sawtooth.

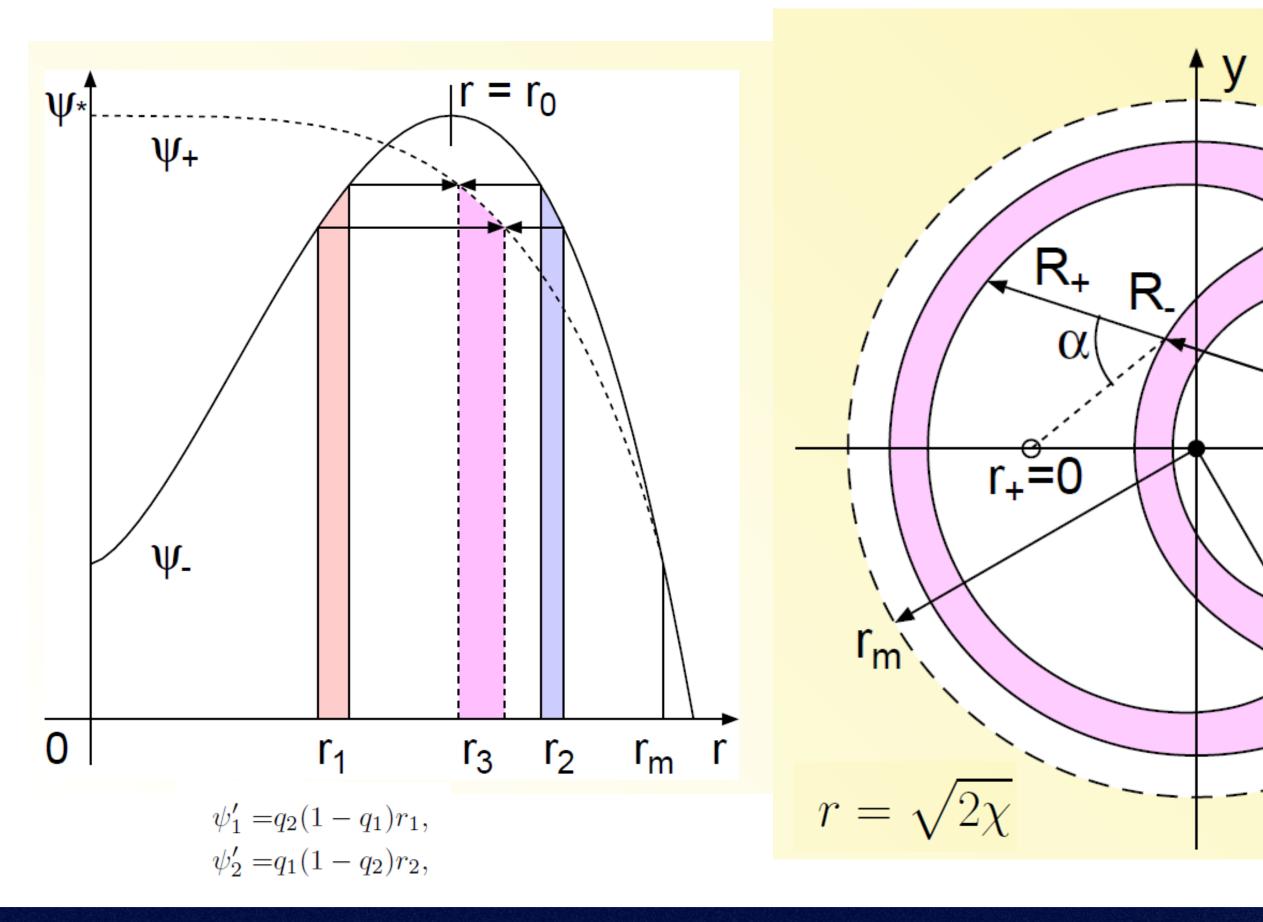






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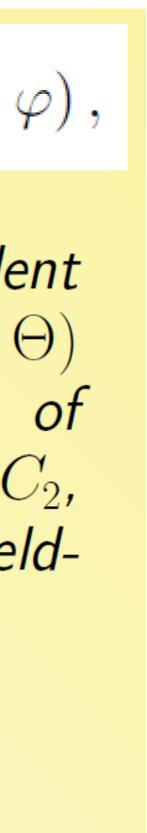


## **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**

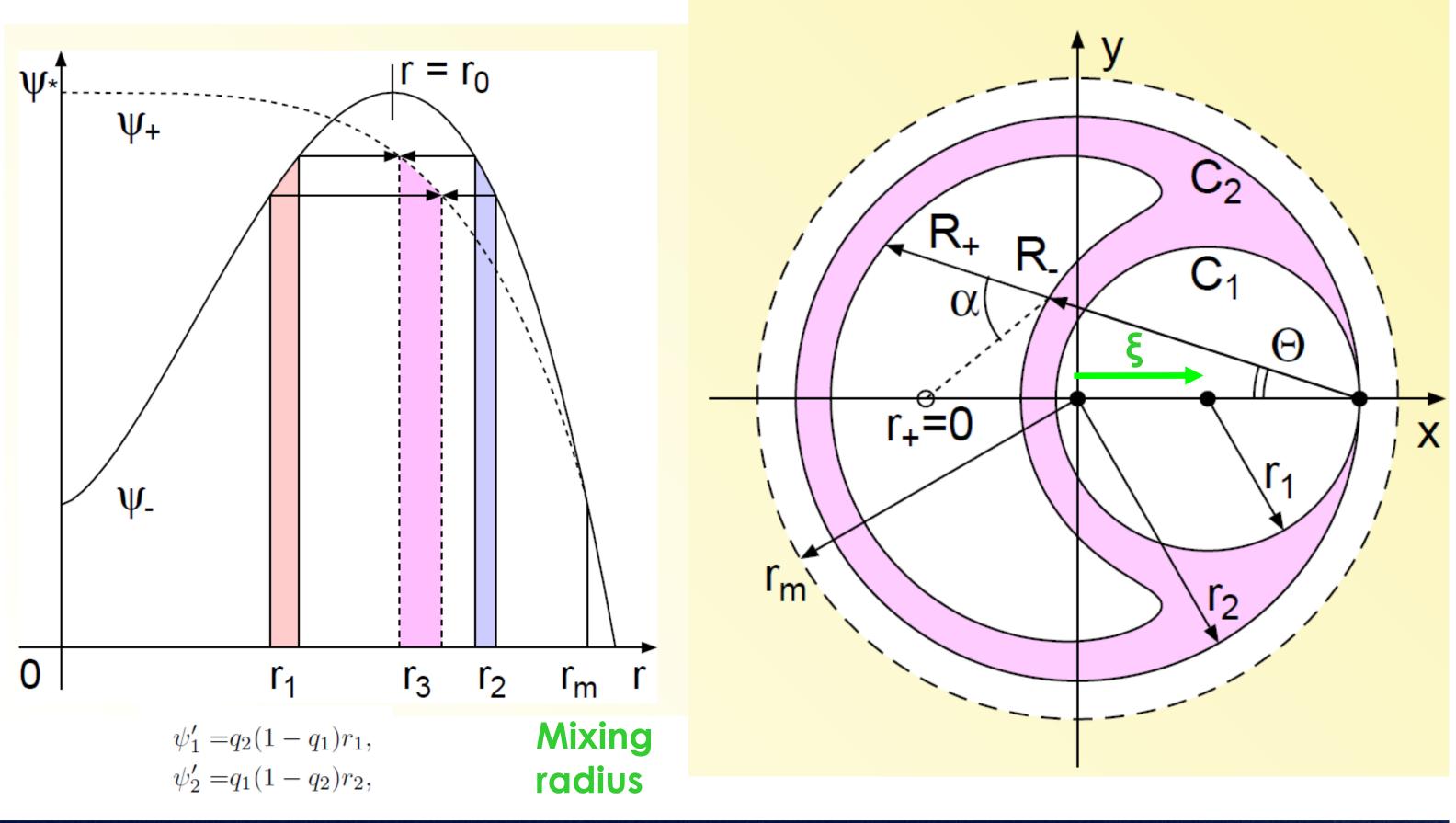
 $\tilde{x} = r \cos(\theta - \varphi)$   $\tilde{y} = r \sin(\theta - \varphi)$ ,

Dimensions and time-dependent polar coordinate system  $(R,\Theta)$ during m = 1 reconnection of magnetic surfaces  $C_1$  and  $C_2$ , shown in the (x, y) straight fieldline coordinate space.









## **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**

<u>3 regions:</u>

- Outer region  $(r > r_2)$  is still unperturbed.
- m=1 shifted, unconnected core of radius  $r_1$ . The displacement of the core is the helical displacement  $\xi$ .

$$\zeta = \sqrt{(\tilde{x} - \xi)^2 + \tilde{y}^2}$$

 Reconnected (island) area, increasing from 0 to  $\pi r_m^2$ .





## Defining the contour within the island

In the reconnected area, we define surfaces  $r_{+} = constant$  defined by

$$r_{+} \equiv r_{3}\sqrt{\rho^{2} + \sin^{2}\Theta},$$

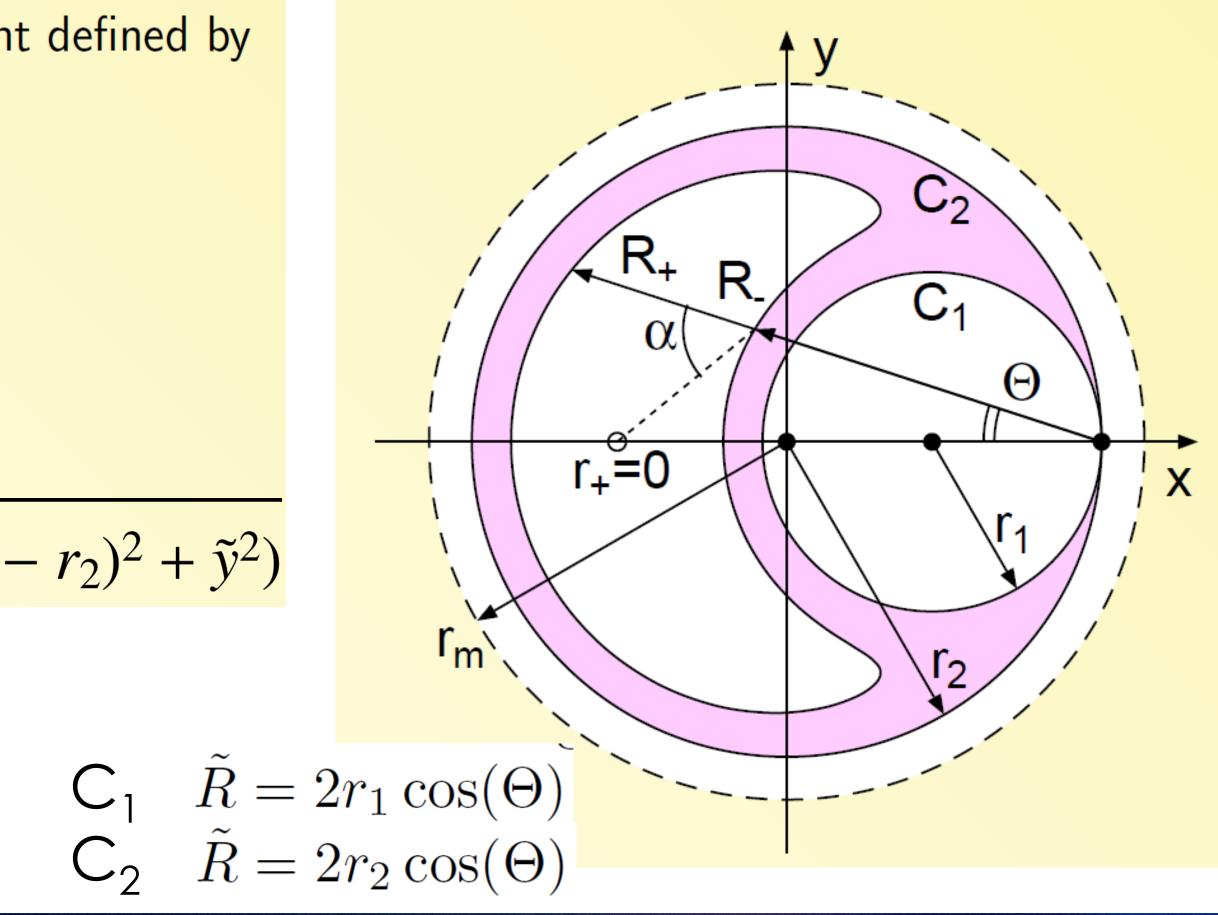
$$\rho \equiv \frac{c\cos\Theta}{1 + \sqrt{1 + (\kappa - \kappa_{r})c}},$$

$$c \equiv \kappa_{r}^{-1} + \kappa - \frac{R^{2}}{r_{3}^{2}\cos^{2}\Theta},$$

$$\kappa_{r} \equiv \frac{r_{2} - r_{1}}{r_{2} + r_{1}}, \qquad \tilde{R} = \sqrt{(\tilde{x} - \kappa_{r})^{2}},$$

Free parameter  $\kappa$  determines the shift of the new magnetic axis. **Properties:** 

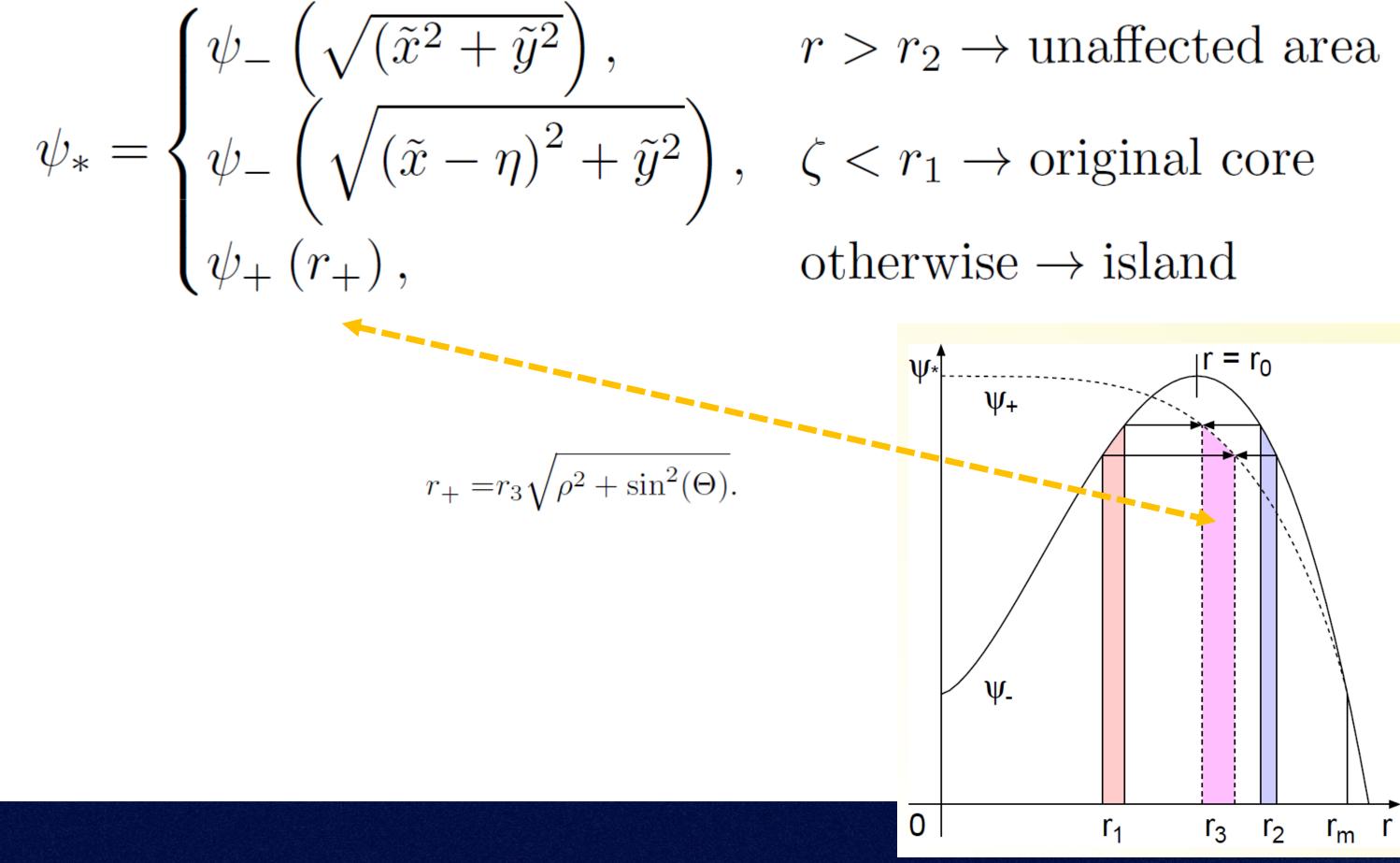
- The cross-section of each contour  $r_{+} = \text{constant}$  has area  $\pi r_{+}^{2}$ .
- $r = r_3$  at the circles  $C_1$  and  $C_2$ , with  $r_3(t) = \sqrt{r_2^2 - r_1^2}$  increasing from 0 to  $r_m$ .
- Allows for a continuous electric potential at  $C_1$  and  $C_2$ .
- **B** is continuous at  $C_1$ ,  $C_2$ for one paramater value  $\kappa = \kappa_c(r_1, r_2)$ .

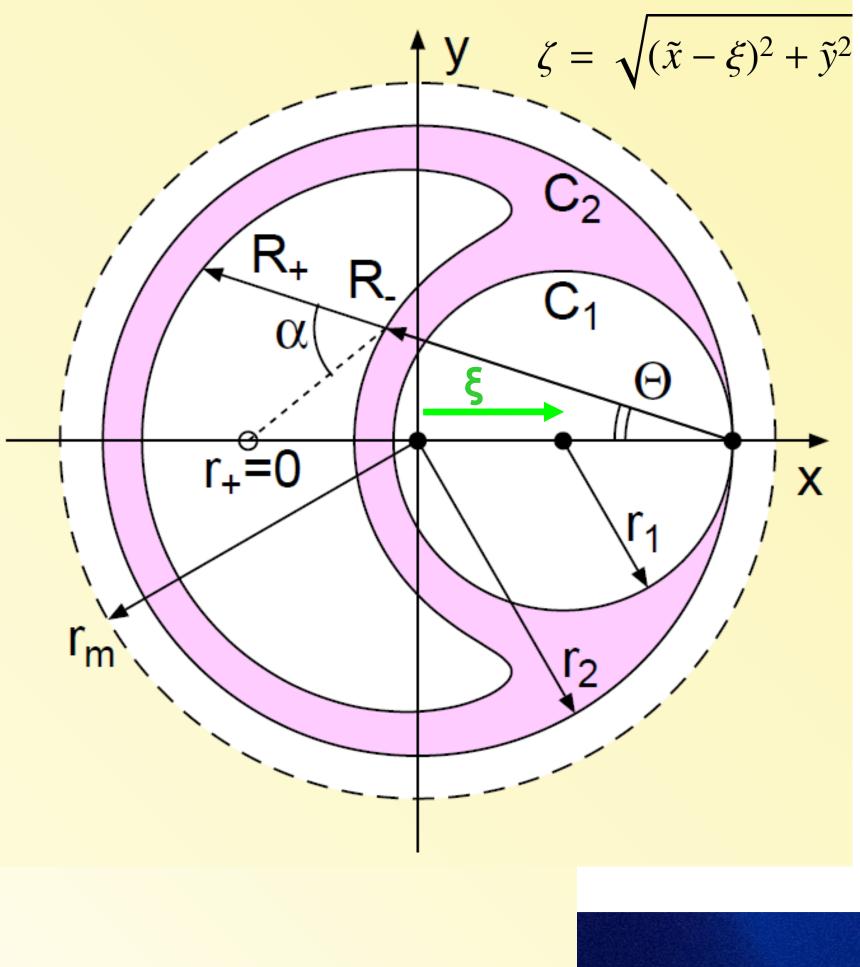






## Defining the magnetic potential

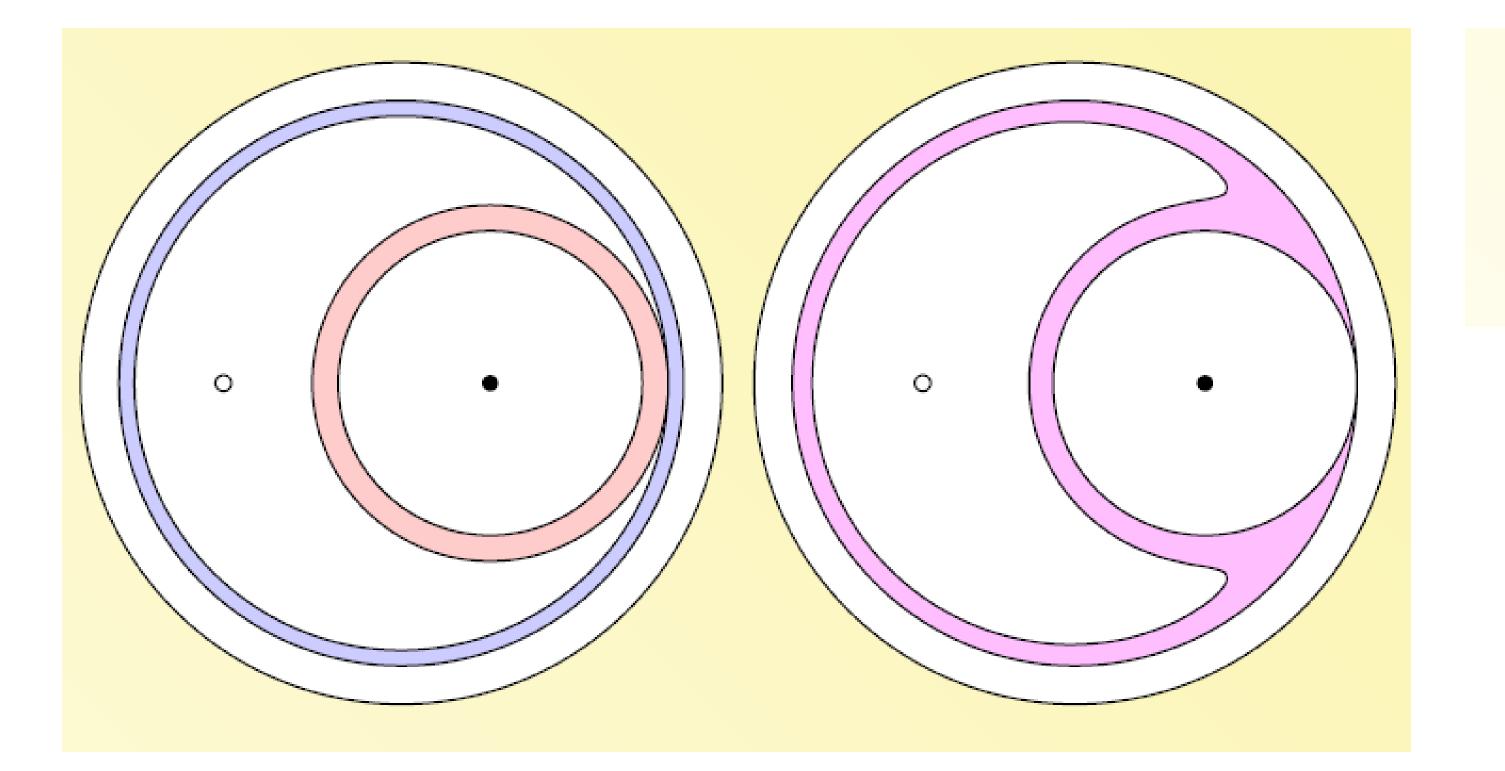








## How to improve the Electric potential calculation?



### **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**

$$\Phi = \Phi_0(\psi_*) + \int_{\psi_*} \frac{\partial \psi_* / \partial t}{|\nabla \psi_*|} dt$$

This integral is the **area in the** (x, y) plane swept out by an arc of fixed  $\psi$ \* while  $\psi$ \*(x, y, t) evolves.







## How to improve the Electric potential calculation?

 $\Phi = \Phi_0(\psi_*) + \int_{\psi_*} \frac{\partial \psi_* / \partial t}{|\nabla \psi_*|} d\ell$ 

### **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**

$$\Phi(\mathbf{x},t) = \Phi_0(r_+) - \int_{C(r_+)} \frac{\partial_t r_+}{|\nabla r_+|} d\ell.$$

$$\Phi = \dot{r_2}\tilde{R}\sin(\Theta) - \frac{\partial}{\partial t}\int_{C(r_+)}\frac{1}{2}\tilde{R}^2\mathrm{d}\Theta,$$

Inside the island







## How to improve the Electric potential calculation?

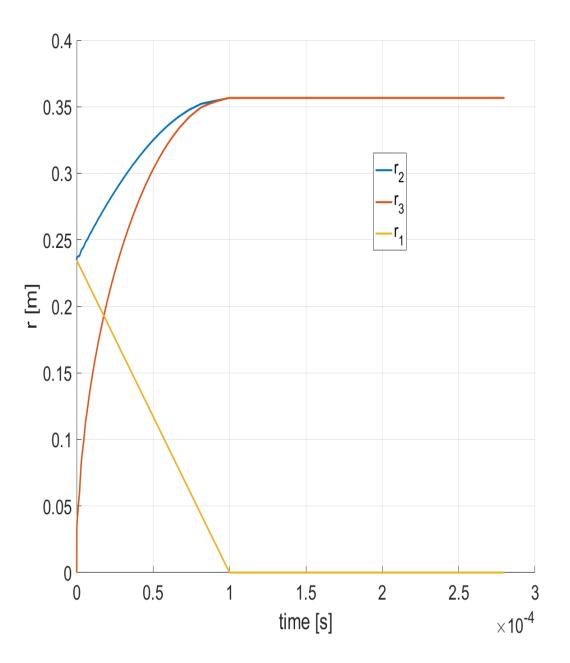
$$\psi_{*} = \begin{cases} \psi_{-} \left( \sqrt{(\tilde{x}^{2} + \tilde{y}^{2})} \right), \\ \psi_{-} \left( \sqrt{(\tilde{x} - \eta)^{2} + \tilde{y}^{2}} \right), \\ \psi_{+} (r_{+}), \end{cases}$$
$$\Phi = \begin{cases} 0, \\ (\dot{r}_{2} - \dot{r}_{1}) \tilde{R} \sin(\Theta), \\ \Theta \left[ \dot{r}_{2} - \dot{r}_{1} \right) \tilde{R} \sin(\Theta), \\ \Theta \left[ \frac{1}{2} \left( r_{+}^{2} - r_{3}^{2} \right) (\dot{\kappa} - \dot{\kappa}_{r}) - \right. \\ + \sin(\Theta) \left[ \dot{r}_{2} \tilde{R} - (r_{1} \dot{r}_{2} + \theta) \right] \end{cases}$$

- $r > r_2 \rightarrow$  unaffected area
- $\zeta < r_1 \rightarrow \text{original core}$
- otherwise  $\rightarrow$  island
- $r > r_2$  $\zeta < r_1$  $+ (\kappa - \kappa_c) r_3 \dot{r_3} ]$   $\cdot r_2 \dot{r_2} \cos(\Theta) + \dot{r_3} r_3 \rho ], \quad \text{otherwise}$

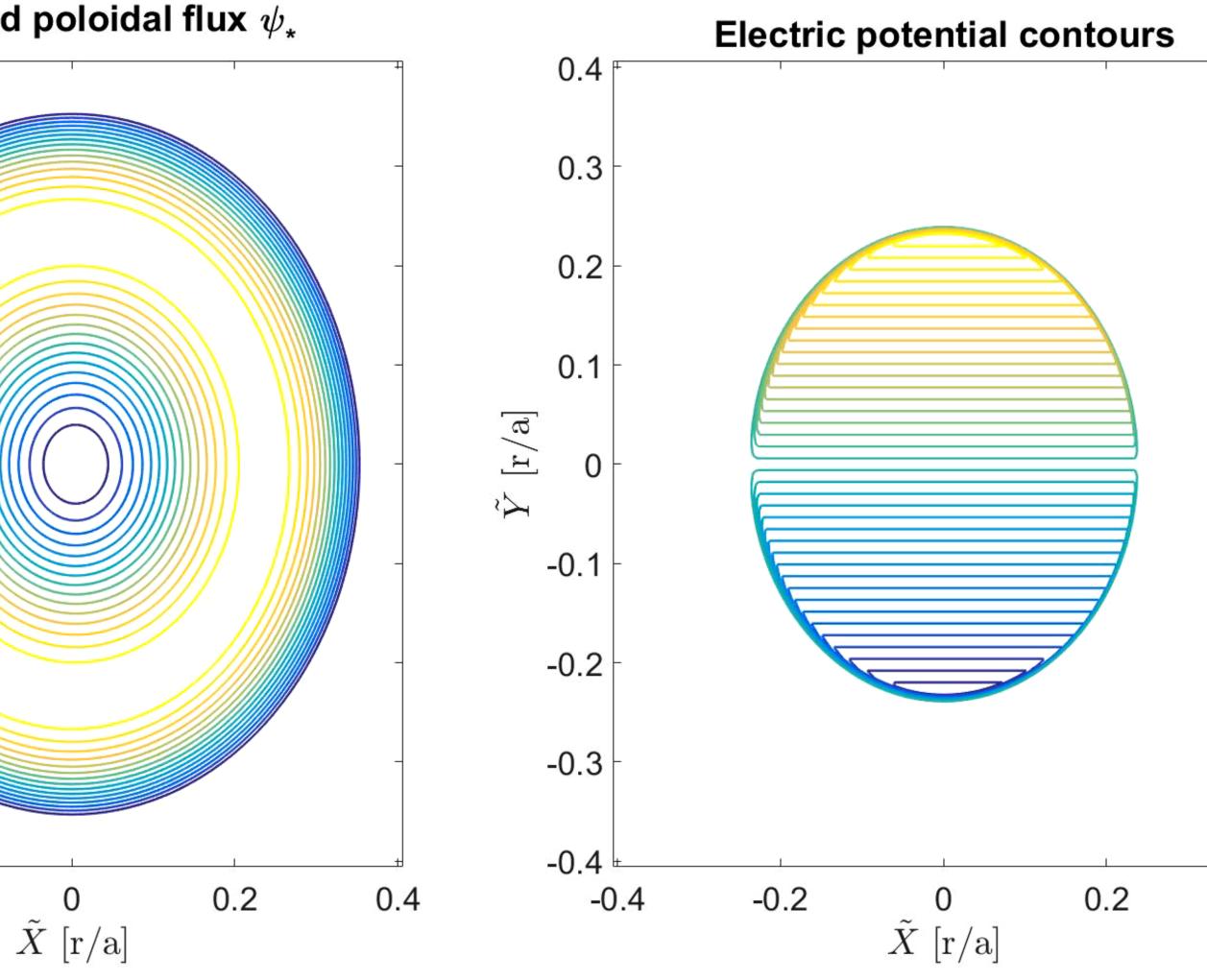








Perturbed poloidal flux  $\psi_*$ 0.4 0.3 0.2 0.1  $\tilde{Y}~[{\rm r/a}]$ 0 -0.1 -0.2 -0.3 -0.4 -0.2 -0.4

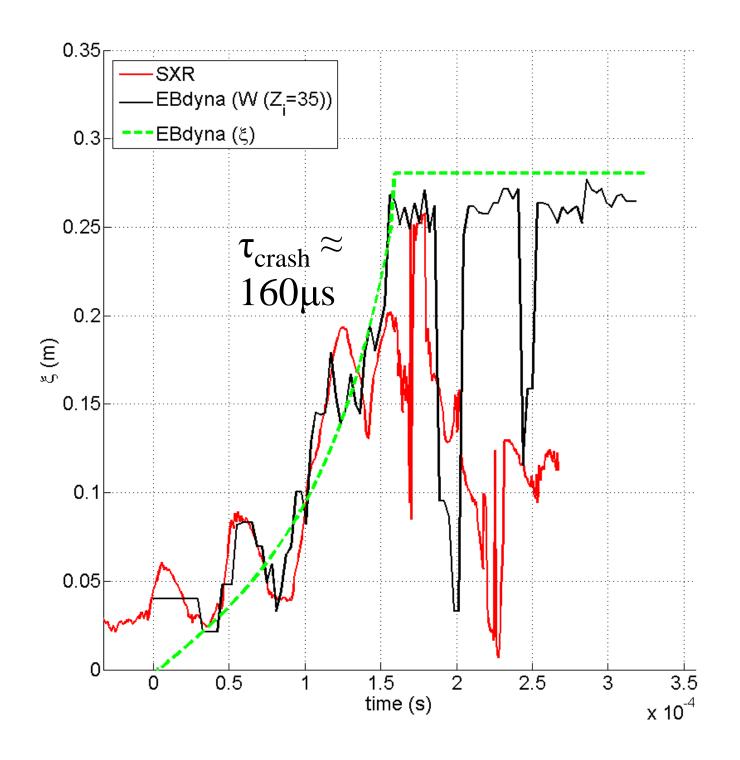








## Illustration of ions motions in sawtooth crash

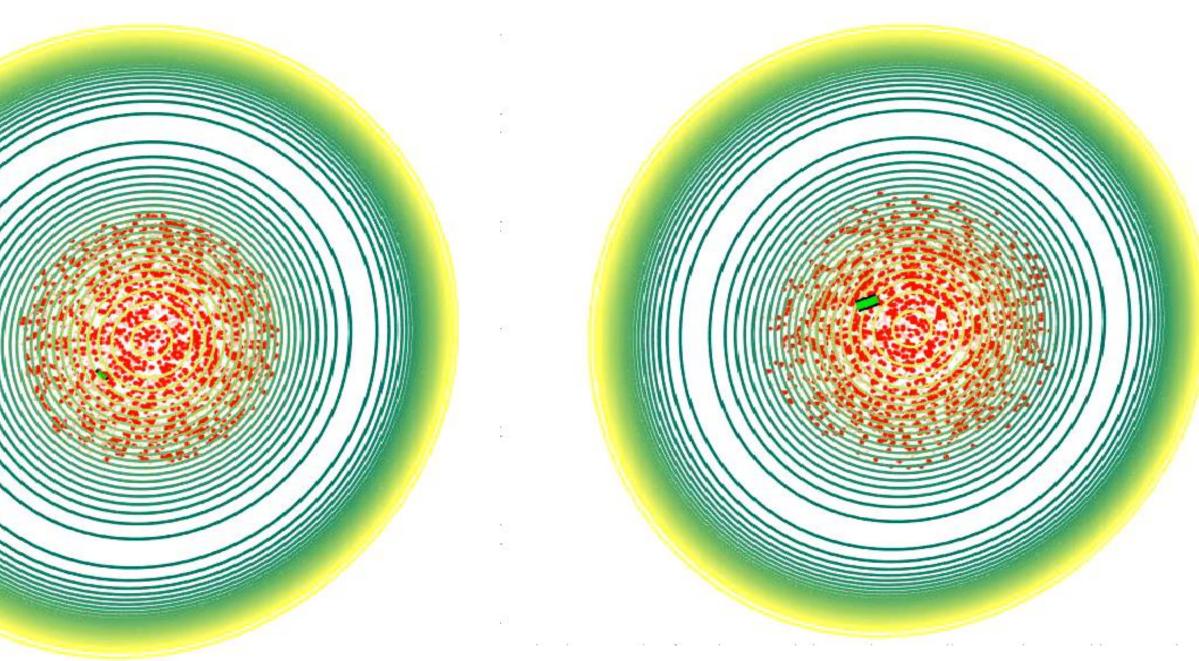


AUG30382 @ 2.5s

Simulation of sawtooth reconnection

25.04.2023

### **COMPUTATIONALLY EFFICIENT POLOIDAL MAPPING OF THE RECONNECTING MAGNETIC FLUX**





Fast D (≈50 keV)









## Summary & outlook

- Safety factor is a critical parameter in order to derive stability of tokamak plasma
- The energy principle allows the derivation of the evolution of plasma in terms of linear stability for a given vector field. For a given test vector field, it is a simple matter of solving several volume integrals.
- Many MHD modes are driven by the local increase of the normalized plasma pressure (β)
- Ideal MHD and sophisticated geometric consideration allowed to derive a computationally efficient poloidal mapping of the reconnecting magnetic flux during a sawtooth crash











## THANK YOU FORYOUR ATTENTION

## OF THE CZECH ACADEMY OF SCIENCES

### FABIEN JAULMES





## Thermonuclear plasma in a tokamak

Change of potential energy:

$$\begin{split} \delta W &= \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_{1}^{2}}{\mu_{0}} + \frac{B^{2}}{\mu_{0}} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^{2} \right. \\ &\left. - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^{*}) - \mathbf{B}_{1} \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j_{\parallel} \right. \\ &\left. + \gamma_{\text{thermo}} P(\boldsymbol{\nabla} \cdot \boldsymbol{\xi})^{2} \right] \mathrm{d} \mathcal{V} \end{split}$$

 $\mathbf{B_1} = \nabla \times (\boldsymbol{\xi}_{\perp} \times \mathbf{B})$ 



### **GY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**

Conservation of the total energy of the plasma yields:

$$\delta W + \delta K = \delta W + \frac{1}{2} \int \rho_i |\dot{\boldsymbol{\xi}}|^2 \mathrm{d} \boldsymbol{\mathcal{V}} = 0$$

Considering an unstable displacement, growth rate  $\gamma_i$ :

$$\boldsymbol{\xi} = \boldsymbol{\xi}_0 \exp(i\omega t) \qquad \qquad \omega^2 = \frac{2\delta W}{\int \rho_i |\boldsymbol{\xi}_0|^2 \mathrm{d} \boldsymbol{\mathcal{V}}} \qquad \qquad \gamma_I^2 = -\omega^2$$

$$\boldsymbol{\xi} = \sum_{m} \boldsymbol{\xi}_{\mathbf{m}}(\psi) \exp[i(m\theta - \varphi)]$$

Considering an approximate circular geometry (neglecting toroidal displacement):

$$\xi_{\theta} = (i/m)\partial(r\xi_r)/\partial r$$







# effect of stabilization of kink by NBI particles

$$\delta W = \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_{1}^{2}}{\mu_{0}} + \frac{B^{2}}{\mu_{0}} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^{2} \right] \mathbf{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^{2} + \mathbf{\Sigma} \mathbf{\delta} \mathbf{k} |^{2}$$

-0.

-0.15

-0.2

-0.25

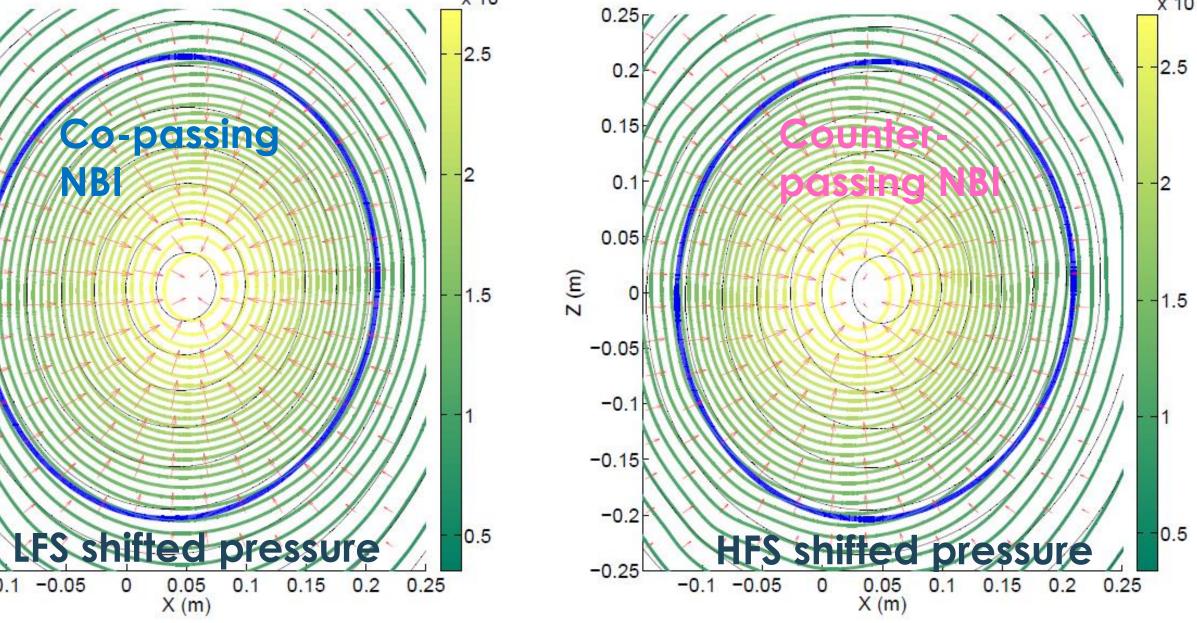
$$\kappa_{pol} = \frac{\mu_0}{B^2} \nabla \left( P + \frac{B^2}{2\mu_0} \right) ;$$
  
$$\kappa_{\varphi} = \left( \frac{(\mathbf{B} \times \nabla B) \times \mathbf{B}}{B^3} \right)_{\varphi} .$$

FIGURE 3.3: Compared pressure contours of the hot NBI population (in a sawtooth equilibrium in ASDEX Upgrade). The arrows indicate the direction of the hot pressure gradient of the NBI population. The left figure corresponds to the experimental case with on-axis co-passing NBI. The right figure corresponds to the same NBI with an opposite parallel velocity. The thick blue line underlines the position of the q = 1 surface.



### **ENERGY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**







47



### **NBI stabilization**

$$\delta W = \frac{1}{2} \int_{\mathcal{V}} \left[ \frac{B_1^2}{\mu_0} + \frac{B^2}{\mu_0} | \boldsymbol{\nabla} \cdot \boldsymbol{\xi}_{\perp} + 2\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\kappa} |^2 - 2(\boldsymbol{\xi}_{\perp} \cdot \boldsymbol{\nabla} P)(\boldsymbol{\kappa} \cdot \boldsymbol{\xi}_{\perp}^*) - \mathbf{B}_1 \cdot (\boldsymbol{\xi}_{\perp} \times \mathbf{b}) j + \gamma_{\text{thermo}} P(\boldsymbol{\nabla} \cdot \boldsymbol{\xi})^2 \right] d\mathcal{V}$$

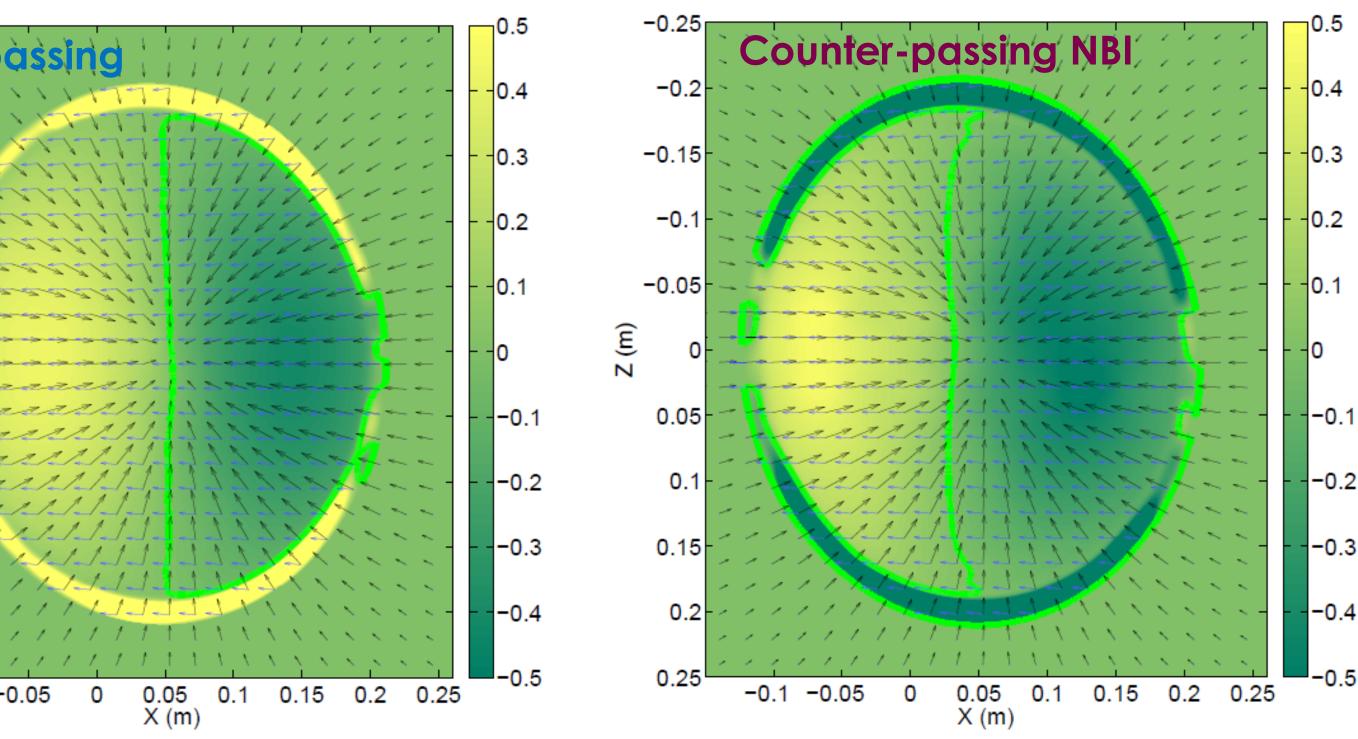
z (m

$$\begin{aligned} \boldsymbol{\kappa_{pol}} &= \frac{\mu_0}{B^2} \boldsymbol{\nabla} \left( \boldsymbol{P} + \frac{B^2}{2\mu_0} \right) \;; \\ \boldsymbol{\kappa_{\varphi}} &= \left( \frac{\left( \mathbf{B} \times \boldsymbol{\nabla} \boldsymbol{B} \right) \times \mathbf{B}}{B^3} \right)_{\varphi} \;. \end{aligned}$$

FIGURE 3.4: Compared values of the normalized potential energy density averaged over the toroidal direction. The left case if a stabilizing co-passing NBI (in a sawtooth equilibrium in AS-DEX Upgrade) and the right one a destabilizing counter-passing situation. The quasi-horizontal blue arrows indicate the curvature  $\kappa$ . The black arrows indicate the gradient of the hot NBI pressure. The thick green lines separates regions of stabilizing and destabilizing contributions. It is readily seen that the region around q = 1 plays an important role for the global stability, because of the large amplitude of the displacement vector there. Around q = 1, the stabilizing or destabilizing sign is induced by the reverse in sign of  $\boldsymbol{\xi} \cdot \boldsymbol{\nabla} P_{hot}$ : in both cases the backward poloidal flow in the q = 1 region is aligned with the equilibrium flux contours; however the angle

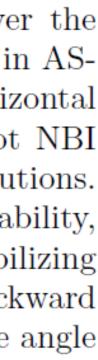
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### **ENERGY PRINCIPLE AND DERIVATION OF LINEAR GROWTH RATE OF INTERNAL KINK**



of the hot pressure gradient with the flux surface is different.







## Reconnecting patterns of $\psi_*$

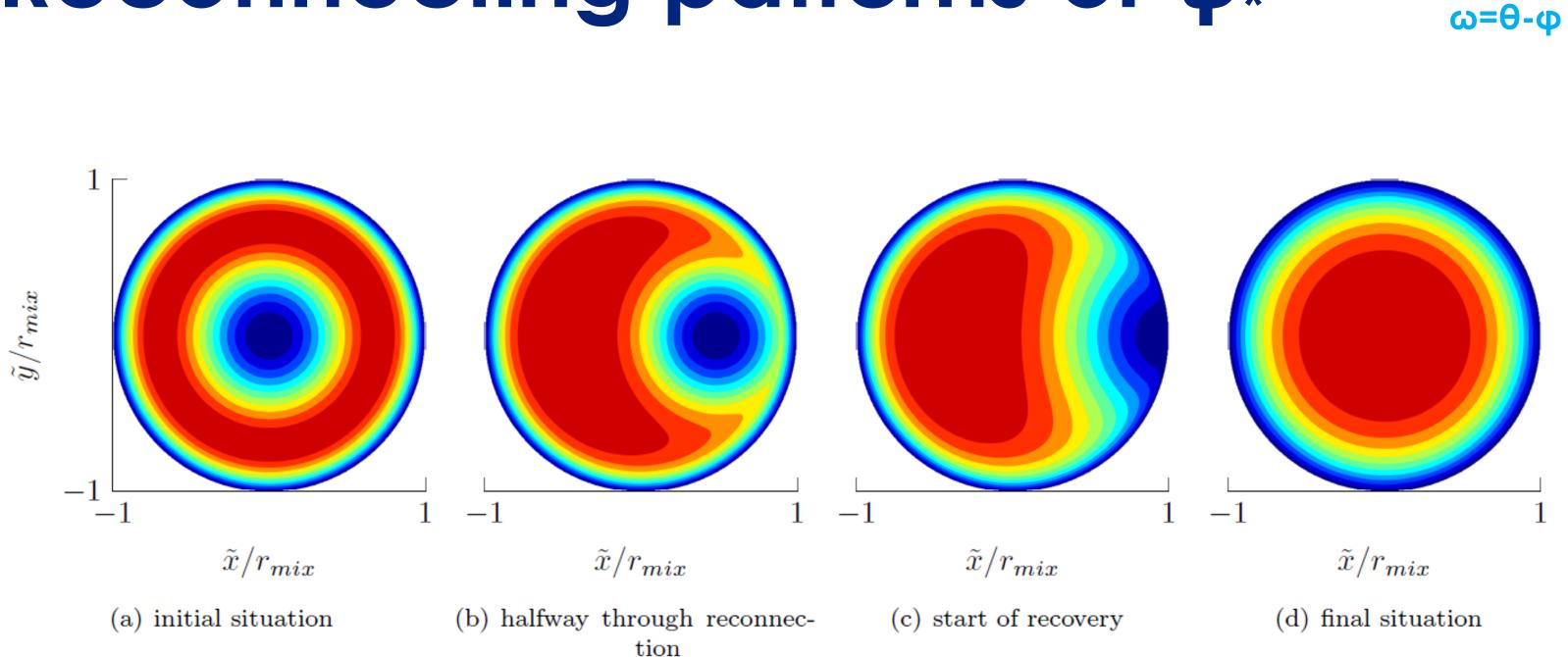
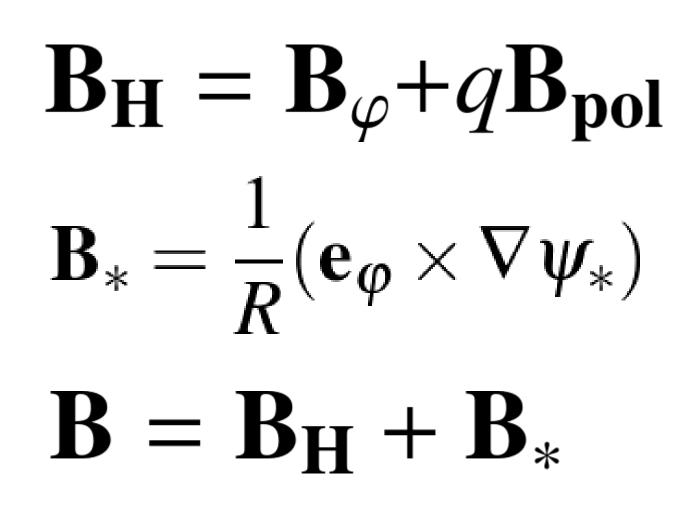


Figure 2.19: Evolution of  $\psi_*$  profile in  $\tilde{x}, \tilde{y}$ -space during collapse with two phases (colors range from 0 to  $\max(\psi_*)$ ). Note that reconnection starts at the 'X'-points at  $r = r_0$  on the q = 1 surface (red in figure 2.19(a)). The 'X'-point moves outwards till  $r = r_{mix}$  (outer blue shell).

#### S. Cats, MSc thesis, 2017

25.04.2023

### **INTRODUCTION TO TOKAMAKS**



Ψ<sub>\*</sub>(r,ω)



